

Site Suitability Report for Civil Design

♥174 Lamb Road, Pukenui, Northland Moekoraha Papakāinga Development

Prepared For:

Realm Property Group Limited

Job No.: 15657

Rev: 0 Date: 29 July 2024



Revision History

Revision No	Description/comments	Prepared By	Date
0	For Resource Consent	P. Liebenberg	29/07/2024

Document Control

Action	Name	Signed	Date
Prepared by	P. Liebenberg		29/07/2024
Ртератей бу	Senior Civil Engineer		29/07/2024
Davioused by	J. Philips	()	20/07/2024
Reviewed by	Technical Manager	James.	29/07/2024

Distribution

Business/company	Attention	Role
Realm Property Group Limited	Alex Hitchcock	Client



Table of Contents

Rev	vision History	2
	cument Control	
Dis	stribution	2
	ole of Contents	
1	Introduction	5
2	Existing Site Description	5
3	Proposed Site Development	
4	Natural Hazards – Flooding	6
	4.1 Council Data – Natural Hazards Mapping & Flood Mapping	7
	4.2 Flood Risk Discussion	7
	4.3 Development Controls	8
5	Earthworks, Erosion and Sediment Control	9
	5.1 Earthworks	9
	5.2 Erosion and Sediment Control (ESC)	
6	Access	
7	Water Supply	
	7.1 Potable Water Supply	
	7.2 Firefighting Water Supply	12
8	Stormwater	13
	8.1 Planning Assessment	13
9	Wastewater	15
	9.1 Site Assessment	15
	9.2 Wastewater System	16
	9.3 Planning Assessment	16
10	Conclusions	18
	10.1 Natural Hazards – Flooding	18
	10.2 Earthworks, Erosion and Sediment Control	18
	10.3 Access	
	10.4 Water Supply	19
	10.5 Firefighting Water Supply	
	10.6 Stormwater	
	10.7 Wastewater	19
11	Limitations	20
12	Appendices	21



Table of Figures

Figure 1: Aerial Image of Development Sites	5
Figure 2: Proposed Site Plan by BDG (Dated 23 July 2024)	6
Figure 3: NRC Site Flood Hazard (NRC Priority Rivers Maps, 10/06/2024)	6
Figure 4: 100-Year Rain-on-Grid Flood map (ICM 26/07/2024)	8
Figure 5: Lamb Road looking east from location of proposed vehicle crossing for communi	ty centre11
List of Tables	
Elot of Tables	
Table 1: Flood Model Inputs	7
Table 2: Estimated Earthwork Volumes	9
Table 3: FNDC Operative Plan - Permitted Activity Assessment	9
Table 4: Proposed Regional Plan for Northland - Permitted Activity Assessment	
Table 5: Proposed Regional Plan for Northland - Permitted Activity Assessment	13
Table 6: Design Occupation (Interpreted from ASNZS 1547:2012, Table J1	16
Table 7: Design flow volume for proposed development	16
Table 8: Land Disposal System Details	
Table 9: FNDC Operative Plan - Permitted Activity Assessment	16
Table 10: Proposed Regional Plan for Northland - Permitted Activity Assessment	17



1 Introduction

Chester Consultants Ltd (Chester) has been engaged by client, Realm Property Group Limited, to provide a Site Suitability Report with respect to proposed residential dwellings on their Papakāinga at 174 Lamb Road, Pukenui, Northland.

This report has been prepared solely for the benefit of this specific project, and the Far North District Council (FNDC). Chester accepts no liability for inaccuracies in third party information used as part of this report. The reliance by other parties on the information or opinions contained in the report shall, without our prior review and agreement in writing, be at such parties' sole risk.

This report is based on development data obtained from the FNDC and Northland Regional Council (NRC) maps current to the site at the time of this document's production. Should alterations be made which impact upon the development not otherwise authorised by this report then the design / comments / recommendations contained within this report may no longer be valid.

In the event of the above, the property owner should immediately notify Chester to enable the impact to be assessed and, if required, the design and or recommendations shall be amended accordingly and as necessary.

2 Existing Site Description

The subject properties are legally described as Section 8 SO 65943, Section 9 SO 65943, these will be referred to as the northern site (Section 9 SO 65943) and southern site (Section 8 SO 65943) respectively in this report.

The property on the southern side is currently vacant. A broad ridgeline traversing from east to west in a zig-zag fashion is present within the northern section of the property. The ridge side slope inclinations range from 20° to 30°. A wetland is present within the northeastern section of the property, between the ridge and the road. The wetland appeared to be dry at time of our site visit. Land to the south of the ridgeline is covered with dense native bush. The eastern section of the ridgeline has been cleared of vegetation and five building platforms and associated accessways have been created.



Figure 1: Aerial Image of Development Sites

The property on the northern side is situated to the north and west of the property on the southern side. A dwelling serviced by a gravel driveway is present near the southeast boundary. Isolated elevated areas are present, including the location of the dwelling platform. The general area is currently used as grazing land.

Refer to Figure 1 above for details of the site and its surrounding features.



3 Proposed Site Development

It is proposed to construct 24 new dwellings across the two sites with associated access roadways, a community centre, and servicing as shown in Figure 2 below and in Appendix A. This report is intended to support a Resource Consent application for Land Use.



Figure 2: Proposed Site Plan by BDG (Dated 23 July 2024)

4 Natural Hazards – Flooding

To assess the flooding risk, we have reviewed the available council flood data and visited the site. Additional Rain-on-Grid (ROG) flood modelling has been undertaken to better determine site specific flooding and overland flowpath extents.

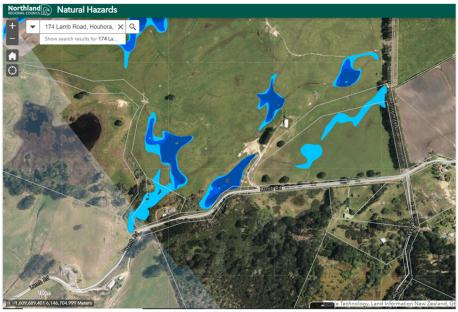


Figure 3: NRC Site Flood Hazard (NRC Priority Rivers Maps, 10/06/2024)



4.1 Council Data - Natural Hazards Mapping & Flood Mapping

As per Figure 3 above, the NRC Natural Hazards Priority Rivers Flood mapping for 10-year, 50 year and 100 year events indicate that there is flooding on the site. However, it is not expected to significantly affect the proposed development as the proposed dwellings will be raised on pile foundations to a level sufficient to provide the minimum freeboard required by Council.

The NRC modelling shows the proposed site is unlikely to be affected by river or coastal inundation flooding but has some localised ponding areas that require additional consideration in our site specific flood modelling.

4.2 Flood Risk Discussion

4.2.1 Site Walkover

From our site walkover we can confirm that the site topography and surrounding catchment is consistent with what is shown on the council flooding maps and from our modelling.

With respect to flooding in the proposed building locations, our site walkover observed no localised depressions or channels of concern given the proposed dwellings will be placed on piled foundations.

4.2.2 Flood Modelling

A 2D Rain-on-Grid (ROG) flood model was created using InfoWorks ICM software to better understand site specific conditions for a typical 1% AEP climate change adjusted storm event. This flood model provided likely extents of localised flooding due to depressions and overland flowpaths within the development area.

Table 1: Flood Model Inputs

rable 1. 1 lood 1 loder inpats	
Model Input	Value
Rainfall Depth (1% AEP, 24hr NIWA Historic)	190mm
Climate Change Factor	20%
Climate Change Rainfall Depth	228mm
Rainfall Hyetograph/Distribution	SCS Type 1A
Terrain Data	NRC LiDAR, 1m DEM
Mannings Roughness	0.035

The flood modelling suggested there are localised area of ponding in excess of 300mm (red zones in Figure 42 below). These local depressions have been identified for earthworks/drainage improvement works during design, to ensure stormwater is drained to the main identified flow channel on site.

The results from the stormwater modelling has identified overland flowpaths (that corresponds to the data from NRC Priority Rivers Maps, 10/06/2024) that need consideration during design and construction. Additionally, the deepest ponding areas identified in red (Figure 42) are caused by low lying land as identified within publicly available LiDAR topographical data. These areas should be avoided for buildings unless specifically designed drainage works are completed, most notably required immediately south of Lamb Road (drain to the stream/pond) and on the western side of Korakanui O Rua Road on the most easterly site boundary.



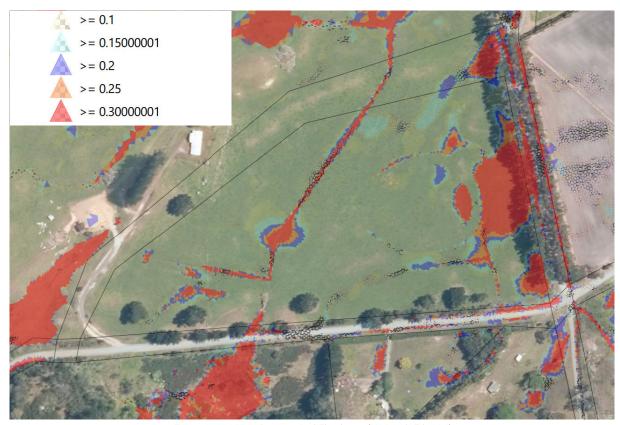


Figure 4: 100-Year Rain-on-Grid Flood map (ICM 26/07/2024)

Given the above, we conclude that NRC priority rivers flood data, complimented with our own stormwater modelling analysis provides a fair representation of the flooding risk on the site which must be considered during design and construction stages of this project.

4.3 Development Controls

Given the nature of the flooding within the development site, we recommend the following building controls.

4.3.1 Dwelling Finished Floor Levels

Proposed dwellings are to maintain a 0.5m (minimum) freeboard above the 1% AEP climate change flood water level perpendicular to the direction of flow at the upstream boundary of a given dwelling as per Far North District Council Engineering Standard 2023, Section 4.3.10.7 Freeboard Requirements.

4.3.2 Foundations and Subfloor Cladding

The proposed dwellings which are to be situated within overland flow path and flood extents are not to impede the overland flow or flooding. As such, the proposed dwellings are required to be situated on pile foundations.

If subfloor cladding is used, then the subfloor cladding is required to allow water to flow through. It is recommended that the cladding is designed so that at least 70% of the surface area is not solid to allow water to flow through. Maintenance hatches are required to be incorporated into the design of the subfloor cladding to provide access to the area underneath the dwellings.

4.3.3 Fencing

New fences proposed within the overland flow path an flooding extents are to comply with the one of the following fence designs:

Post-and-wire or wire mesh type fences;



• Railing type fences where at least 70% of the surface area of the fence is open to allow water to flow through.

4.3.4 Earthworks

Additional earthworks within the development area, beyond what is shown in this proposal, must be designed by a suitably qualified engineer with respect to the flood data presented within this report and the governing standards at the time of future assessment.

4.3.5 Structures and Utility Servicing

Structures, including foundations, are to be made out of water-resistant construction materials and are to be structurally designed to withstand flood forces during the 1% AEP flooding event.

Utility service connections are to be constructed to ensure flood-proofing should they become submerged within the overland flow or flood extents.

5 Earthworks, Erosion and Sediment Control

5.1 Earthworks

Earthworks are required to upgrade the private accessway and provide services for the site. The proposed works will not be within the permitted activity requirements as per the FNDC District Plan section 12.3.6.1.1 and the Proposed Regional Plan for Northland C.8.3.1.

5.1.1 Expected Earthwork Volumes

Table 2 below outlines the estimated earthworks volumes.

Table 2: Estimated Earthwork Volumes

Earthwork	Value
Disturbed Area	20,350 sq-m
Cut Volume	2700 cu-m
Fill Volume	5650 cu-m
Net Earthworks	2950 cu-m (Fill)

5.1.2 FNDC Operative District Plan Earthwork Assessment

We have prepared an assessment as per the Far North District Council Operative Plan. Table 3 below sets out the relevant rules and assessments under Section 3, Chapter 12 of the Plan.

Table 3: FNDC Operative Plan - Permitted Activity Assessment

Table 3. INDC Operative Flair Terrificed Activity Assessment	
Rule 12.3.6.1.1	Assessment/Comment
12.3.6.1.1 Land use Activities Involving Excavation	The estimated earthwork volume exceeds 5,000
and/or filling, excluding mining and quarrying, in the	cubic metres with 2700 cu-m of Cut and 5650 cu-
Rural Production Zone or Kauri Cliffs Zone.	m of Fill. Thus the earthwork activities in this
	proposal are not a permitted activity.
Excavation and/or filling, excluding mining and	
quarrying, on any site in the Rural Production Zone or	
Kauri Cliffs Zone is permitted, provided that:	
a. It does not exceed 5,000m³ in any 12-	
month period per site; and	
b. It does not involve a continuous cut or filled	
face exceeding an average of 1.5m in height	
over the length of the face i.e., the maximum	
permitted average cut and fill height may be	
3m.	



5.1.3 NRC Proposed Regional Plan Earthwork Assessment

We have prepared an assessment as per the Proposed Regional Plan for Northland, February 2024. Table 4 below sets out our assessment against section C.8.3.1 Earthworks.

Rule C.8.3.1: the area and volume of earthworks at a particular location or associated with a project complies with the thresholds in [NRC Regional Plan] Table 15: Permitted activity earthworks thresholds.

Table 4: Proposed Regional Plan for Northland - Permitted Activity Assessment

Table 4: Proposed Regional Plan for Northland	<u>d - Permitted Activity Assessment</u>	
Location	Earthworks Thresholds	Assessment/Comment
Within 10m of a natural wetland, the bed of a continually or intermittently flowing river or lake	200 square metres of exposed earth at any time, and 50 cubic metres of moved or placed earth in any 12-month period.	No earthworks are proposed within 10m of a natural wetland.
Within 10m of an īnanga spawning site	200 square metres of exposed earth at any time, and 50 cubic metres of moved or placed earth in any 12-month period.	The development site is not within 10m of an īnanga spawning site.
Catchment of an Outstanding Lake	2500 square metres of exposed earth at any time.	The development site is not within a catchment of an outstanding lake.
Erosion-prone Land	2500 square metres of exposed earth at any time.	The development site is not within the Erosion Prone Land overlay.
High-risk flood hazard area	50 cubic metres of moved or placed earth in any 12-month period.	Not applicable.
Coastal riparian and foredune management area	Excluding for coastal dune restoration, 200 square metres of exposed earth at any time.	The development site is not in a coastal area.
Flood hazard area	100 cubic metres of moved or place earth in any 12-month period.	Earthworks of ±90 cu-m related to the roadway construction are proposed within a flood hazard area.
Other areas	5,000 square metres of exposed earth at any time.	The proposed earthworks area for the site more than 5,000m ² .

5.2 Erosion and Sediment Control (ESC)

Erosion and sediment control (ESC) measures can be implemented to reduce the amount of sediment generated, prior to the commencement of vegetation clearance and earthworks. Specific management and implementation of erosion and sediment control may be used including:

- Undertaking earthworks and construction during the drier summer months to minimise likelihood of heavy rainfall and extended periods of rainfall.
- Minimising duration and amount of exposed earth.
- Installation of sediment control bunds to divert clean water around the exposed earth site.
- Installation of silt fences/super silt fences in accordance with section F1.3/F1.4 of Auckland Council Guidance Document 005 (GD05).
- Installation of silt socks in accordance with section F1.5 of GD05.

Therefore, we can conclude that the minor earthworks required to complete the development enabling works are a permitted activity under the FNDC District Plan. Sediment control bunds and/or silt fences and/or silt socks are to be implemented prior to physical earthworks being undertaken.



6 Access

6.1 Vehicle Crossing

Vehicle crossings provide a means of vehicular access to a property as a vehicle moves from the roadway, across the berm, and into a property.

6.1.1 Existing Crossing

The project site shares a legal boundary with the Lamb Road reserve and thus has a legal means of access to and from the property, however, the northern site and southern site are currently not provided with vehicle crossings.

6.1.1 Proposed Crossings

It is proposed to construct three new vehicle crossings to provide access to the new development off Lamb Road.

One crossing for the common access way for the northern site.

One crossing for the common access way for the southern site.

One crossing for access to the community centre on the northern site, located on the shared boundary between Section 9 SO 65943, Section 8 SO 65943 & Lamb Road (Par ID 5209513).

The vehicle crossings are proposed to be in general accordance with FNDC Engineering Standards (Sheet 21 Type - 1B).

The existing environment at the proposed location of the community centre's access fails to provide adequate sightlines to the east of the proposed vehicle crossing along Lamb Road because of vegetation—refer to Figure 5 below. Clearing of vegetation will be necessary to achieve suitable sightlines.

Refer to the Civil Design 700 plans prepared by Chester for more information.



Figure 5: Lamb Road looking east from location of proposed vehicle crossing for community centre



6.2 Private Accessway

It is proposed to construct two new shared accessways within the sites to provide access to the twenty four new dwellings. The accessways are proposed to be in general accordance with FNDC District Plan standards for private access.

Refer to the Civil Design 700 plans prepared by Chester Consultants for more information.

7 Water Supply

There is no public reticulated water supply available to the site.

7.1 Potable Water Supply

It is proposed to install on-site water tanks to service the proposed development in terms of potable water supply, which is typical in the surrounding rural area. At the time of the building consent application for the proposed new dwellings, the rainwater tanks will be designed to meet the demands of each dwelling and its occupants.

Refer to the Civil Design 600 plans prepared by Chester Consultants for more information.

7.2 Firefighting Water Supply

It is proposed to provide on-site firefighting water supply in accordance with SNZ PAS 4509:2008. Fire water supply will be provided from on-site water storage tanks.

7.2.1 Fire Water Demand

As per Standard New Zealand Publicly Available Specification 4509 (SNZ PAS 4509:2008), non-sprinklered single family and multi-unit dwellings (excluding multi-story apartments) require fire water supplies classified as FW2.

To meet the requirement of FW2, on-site fire water storage tanks must meet the following requirements:

- Storage of 45 cubic metres to provide firefighting water supply for 30 minutes not more than 90 metres and no closer than 6 metres from the fire hazard;
- Unimpeded vehicular access to the storage location with roading able to support a 20 tonne vehicle:
- Storage to be vertically and horizontally located even with and adjacent to the vehicular hardstand to limit suction lift and friction losses for the firefighting pump;
- Means to automatically keep the tank topped up and manually refilled after emptying;
- Lengths listed above shall generally be considered as the length of hose as it lies on the ground;
- Refer to SNZ PAS 4509:2008 for additional requirements and information.

7.2.2 Fire Water Supply Locations

On-site water storage, in compliance with SNZ PAS 4509:2008, will consist of two 25m³ water tanks to be located at various locations to meet the maximum distance requirement of 90m from the proposed properties. It will be topped up and have water circulated from the roof of nearby dwelling(s) and be fitted with a screw coupling adaptor and shut off valve at the base.

Refer to the Civil Design 600 plan prepared by Chester Consultants for a layout of the proposed locations.



8 Stormwater

There is no public stormwater network available to the site. Currently stormwater appears to discharge to the natural ground and sheet flow towards the northeast corner of the northern site.

Stormwater runoff from the dwelling roofs are proposed to be collected into re-use water tanks and used for potable water supply. Overflow from the tanks will be discharged to the surrounding area. The outlet of the overflow will have rip rap to provide suitable erosion protection where required.

To collect stormwater surface runoff from the private accessway on the southern site, privately owned and maintained catchpits will be provided at the low points of the accessways to capture sediment prior to discharge at the base of the hillsides. At the base of the hillsides, erosion protection/energy dissipation will be provided prior to the runoff flowing across the ground and following historic drainage patterns.

Stormwater surface runoff from the private accessway on the northern site will be collected and diverted within an open drain adjacent to the road where sediment will be captured before discharging to the natural ground surface and following historic drainage patterns.

The impervious area of the proposed development is less than the maximum allowable impervious area of 15%.

Refer to the Civil Design 400 plans prepared by Chester for more information.

8.1 Planning Assessment

8.1.1 NRC Proposed Regional Plan Stormwater Assessment

Table 5 below sets out our assessment against section C.6.4.2 Other stormwater discharges – permitted activity of the Proposed Regional Plan for Northland, February 2024. In our opinion, the diversion and discharge of stormwater appears to comply with the Permitted activity status.

Table 5: Proposed Regional Plan for Northland - Permitted Activity Assessment

Table	5: Proposed Regional Plan for	Northland - Permitted Activity Ass	essment
Rul	e C.6.4.2		Assessment/Comment
1.	·	sion is not from: nwater network, or lustrial or trade premises,	The discharge is not from a public stormwater network or high-risk industrial or trade premises.
2.	increase flooding of lar storm event of up to a annual exceedance pro	·	In our opinion, the discharge will not cause or increase flooding on another property. Although the post-development impervious area is larger than the pre-development, the runoff is being discharged to the same catchment.
3.	 a. the stormwater content and operated to pure substances stored entering the storm b. there is a secondar place to intercept substances and either the storm of the store of the stor	torage or handling area: bllection system is designed revent hazardous or used on the site from hwater system, or ry containment system in any spillage of hazardous ther discharges that spillage ystem or stores it for	The discharge is not from a hazardous substance storage or handling area.



С.	if the stormwater contains oil contaminants,
	the stormwater is passed through a
	stormwater treatment system designed in
	accordance with the Environmental
	Guidelines for Water Discharges from
	Petroleum Industry Sites in New Zealand
	(Ministry for the Environment, 1998) prior to
	discharge, and

4. Where the diversion or discharge is from an industrial or trade premises:

The discharge is not from an industrial or trade premises.

- a. the stormwater collection system is designed and operated to prevent any contaminants stored or used on the site, other than those already controlled by condition 3) above, from entering stormwater unless the stormwater is discharged through a stormwater treatment system, and
- b. any process water or liquid waste stream on the site is bunded, or otherwise contained, within an area of sufficient capacity to provide secondary containment equivalent to 100 percent of the quantity of any process water or liquid waste that has the potential to spill into a stormwater collection system, in order to prevent trade waste entering the stormwater collection system, and
- The diversion or discharge is not into potentially contaminated land, or onto potentially contaminated land that is not covered by an impervious area, and

The discharge is not into potentially contaminated land, or onto potentially contaminated land that is not covered by an impervious area.

6. The diversion and discharge does not cause permanent scouring or erosion of the bed of a water body at the point of discharge, and

Erosion and scour protection is proposed at the point of discharge.

7. The discharge does not contain more than 15 milligrams per litre of total petroleum hydrocarbons, and

The proposed impermeable areas are all low contaminant yielding and are very unlikely to pick up petroleum hydrocarbon contaminants of more than 5 milligrams per litre.

None of these effects are anticipated on the

8. The discharge does not cause any of the following effects in the receiving waters beyond the zone of reasonable mixing:

of receiving waters.

- a. the production of conspicuous oil or grease films, scums or foams, of floatable or suspended materials, or
- b. a conspicuous change in the colour or visual clarity, or
- c. an emission of objectionable odour, or
- d. the rendering of freshwater unsuitable for consumption by farm animals, or
- e. the rendering of freshwater taken from a mapped priority drinking water

abstraction point (refer I Maps | Ngā mahere matawhenua) unsuitable for human consumption after existing treatment.

9 Wastewater

The development site does not have a connection to the existing public network. As such, on-site wastewater treatment and disposal is proposed. A site assessment has been undertaken by Soil and Rock Consultants which has been used to develop an indicative design for an on-site dispersal field in accordance with ASNZS 1547:2012 and the Proposed Regional Plan for Northland. The following sections summarises our assessment and indicative design which will be further developed at the detailed design stage.

9.1 Site Assessment

A desktop study and geotechnical investigations of the development site were completed by Soil and Rock Consultants. Reference to the GNS New Zealand Geological Web Map 1:250,000 Geology map indicates the site is underlain by dune sand deposits of the Karioitahi Group (See Figure 3). Karioitahi Group soils are described as weakly cemented sand in fixed parabolic dunes with intermixed sand, mud, and peat in interdune deposits.

Loose to cemented sands were encountered during the investigation, with no mud or peat deposits encountered (apart from one auger hole, which showed organic-stained sand, drilled within the wetland area).

The near-surface soils can be classified as Soil Category 3 (medium-fine and loamy sand – good drainage) as per Auckland Council Technical Publication 58 (TP58). However, for conservativity, it is recommended that Soil Category 4 (sandy loam – moderate drainage), with a maximum dispersal rate of 5mm/day, be adopted for wastewater design. Given the dense, less permeable soil at shallow depth, dispersal via conventional in-ground soakage trenches should be avoided - dispersal of treated wastewater would best be achieved via Pressure-Compensated Dripline Irrigation (PCDI) on a raised bed to ensure separation from seasonal high groundwater.

Please refer to the Geotechnical Investigation Report prepared on the 5th of April 2024 by Soil and Rock Consultants for further details.

9.1.1 Groundwater

Groundwater was not encountered in most of the auger holes on the day of drilling, with the exception of one auger hole where groundwater was measured at 1.1m bpgl. Groundwater measurements taken during drilling are not always an accurate portrayal of the actual long-term groundwater table as groundwater levels can take time to stabilise within the auger hole following drilling.

It is therefore recommended that the dispersal beds be raised to ensure separation from seasonal high groundwater.

9.1.2 Design Flow Volume

The following section sets out the design flow volume for the proposed wastewater disposal system based on the proposed development shown in <u>Figure 2</u> above.



Table 6: Design Occupation (Interpreted from ASNZS 1547:2012
--

No. of Bedrooms	No. of Dwellings	Population Equivalent	Design Occupancy					
Northern Site								
2	4	4	16					
3	6	5	30					
4	9	6	54					
Community Centre	1	50	50					
Kohanga Reo	1	35	35					
		Total:	185					
No. of Bedrooms	No. of Dwellings	Population Equivalent	Design Occupancy					
Southern Site								
2	8	4	32					
3	3	5	15					
		Total:	47					

Table 7: Design flow volume for proposed development

Four Bedroom Dwelling:	
Design Occupancy:	185 (North) and 47 (South) (Table 6 above)
	145 L/person/day (ASNZS 1547:2012, Table H3, Standard
Design Flow Allowance per Person:	Water Reduction Fixtures, Water Tank Supply)
Design Flow Allowance per Person.	20 L/person/day for community centre (ASNZS 1547:2012,
	Table H4, Standard Water Fixtures, Water Tank Supply)
Design Flow Volume:	16,200 L/day (North) and 6815L/day (South)

9.2 Wastewater System

9.2.1 Treatment System

The treatment system required for this design is proposed to be for secondary wastewater treatment and treat a design flows of 16200 L/day (North) and 6815L/day (South), outlined in Table 7 above. The system supplier is to be determined at the detailed design stage.

9.2.2 Land Disposal System

Table 8: Land Disposal System Details

Land Disposal	
Disposal Method:	Pressure-Compensated Dripline Irrigation
Selected Loading Rate:	5 mm/day (Category 4 soils, ASNZS 1547:2012, Table L1)
Disposal Field Area:	16,200/5 = 3,240m ² north and 6,815/5 = 1,363 m ² south
Reserve Area:	972m² for north and 409 for south (30%, NRC Regional Plan.
Reserve Area.	Section C.6.1.1)
Total Area Required:	4212m ² for north and 1,772 m ² for south
Bed depth:	0.6m min.
Topsoil Depth:	100-150mm (to be designed by others)
Servicing Requirement:	As per manufacturers specifications

Refer to Chester Drawing 520 and 521 for the proposed location of the treatment and disposal system.

9.3 Planning Assessment

This section of the report sets out our assessment of the proposed activity against the relevant planning rules.

9.3.1 Far North District Council Operative Plan

Chester Consultants believe that the proposal is a permitted activity under Far North District Council Operative Plan. Table 9 below sets out the relevant rule under Section 7, Chapter 12:

Table 9: FNDC Operative Plan - Permitted Activity Assessment



Rule 12.7.6.1.4

Land use activities which produce human sewage effluent (including grey water) are permitted provided that:

- a. the effluent discharges to a lawfully established reticulated sewerage system; or
- b. the effluent is treated and disposed of onsite such that each site has its own treatment and disposal system no part of which shall be located closer than 30m from the boundary of any river, lake, wetland or the boundary of the coastal marine area.

Assessment/Comment

The waste created by the development is proposed to be treated and disposed of by a system which has no part closer than 30 m from the bank of any river, lake, wetland, or the boundary of the coastal marine area.

9.3.2 Proposed Regional Plan for Northland

Table 10 below sets out our assessment against section C.6.1.3 Other on-site treated domestic wastewater discharge – permitted activity of the Proposed Regional Plan for Northland, February 2024.

Table 10: Proposed Regional Plan for Northland - Permitted Activity Assessment

		sed Regional Plan for Northland - Permitted Activity Ass				
	le C.6.1.		Assessment/Comment			
1.	accord Standa	-site system is designed and constructed in ance with the Australian/New Zealand rd. On-site Domestic Wastewater ement (AS/NZS 1547:2012), and	The on-site wastewater system has been designed in accordance with AS/NZS 1547:2012.			
2.		lume of wastewater discharged does not two cubic metres per day, and	The maximum daily design flow volume is 23 cubic metres per day which is more than 2 cubic metres.			
3.		charge is not via a spray irrigation system o soakage system, and	The discharge is via a drip irrigation system.			
4.	25 deg	pe of the disposal area is not greater than rees, and	The max slope is approximately 0.5% (north) and 2.5% (south).			
5.		stewater that has received secondary or treatment, it is discharged via: a trench or bed system in soil categories 3 to 5 that is designed in accordance with Appendix L of Australian/New Zealand Standard On-Site Domestic Wastewater Management (AS/NZS 1547:2012); or an irrigation line system that is dose loaded and covered by a minimum of 50 millimetres of topsoil, mulch, or bark, and	The wastewater will receive secondary treatment and is disposed of into Category 4 equivalent soils via a Pressure-Compensated Dripline Irrigation system.			
6.		discharge of wastewater onto the surface es greater than 10 degrees: the wastewater, excluding greywater, has received at least secondary treatment, and the irrigation lines are firmly attached to the disposal area, and where there is an up-slope catchment that generates stormwater runoff, a diversion system is installed and maintained to divert surface water runoff from the up-slope catchment away from the disposal area, and	The proposed disposal system discharges onto a slope shallower than 10 degrees, so this does not apply.			

The proposal complies with all exclusion areas and setback distances set out in [FNDC District Plan] Table 9.
The proposed system will have a filter that meets this requirement.
The wastewater receives secondary treatment system and a 30% reserve area is proposed.
A maintenance agreement between the applicant and supplier (or other suitably qualified contractor) is to be entered in to.
Noted.
Noted.
Noted.

9.3.3 Water Conservation Condition

Chester Consultants recommends that it be a condition of consent that the houses are fitted with standard water reduction fittings to ensure that fact is not lost upon home builders with respect to onsite wastewater disposal system.

10 Conclusions

10.1 Natural Hazards - Flooding

The proposed dwellings will be placed on pile foundations with minimum freeboard of 500mm from finished floor to flood water level.

10.2 Earthworks, Erosion and Sediment Control

Earthworks are proposed to in relation to the road construction within the site. Sediment control measures (bunds, silt fences and or silt socks) are to be implemented prior to physical earthworks being undertaken.



10.3 Access

The existing properties don't have access to the public road reserve and three new vehicle crossings are proposed (two for the northern site and one for the southern site). Two common access ways are required to provide access to the proposed dwellings.

10.4 Water Supply

The existing property does not have access to the public water supply service. On-site rainwater tanks are proposed to service the new development for potable water supply.

10.5 Firefighting Water Supply

The existing property requires fire water supplies sufficient to satisfy the FW2 requirements. It is proposed to provide the new development with on-site water storage for firefighting purposes no more than 90m from a given dwelling.

10.6 Stormwater

The existing property does not have access to the public stormwater service. Roof runoff will be collected and used for potable water supply. Runoff from the accessways will be collected via private catchpits or swales to capture sediment prior to discharge to ground so it may follow historic drainage patterns.

10.7 Wastewater

The existing property does not have access to the public wastewater service. It is proposed to service the development via an on-site wastewater treatment and land disposal system in accordance with ASNZS1547:2012. The design flow volume is less than 2m³/day.



11 Limitations

This assessment contains the professional opinion of Chester Consultants as to the matters set out herein, in light of the information available to it during the preparation, using its professional judgement and acting in accordance with the standard of care and skill normally exercised by professional engineers providing similar services in similar circumstances. No other express or implied warranty is made as to the professional advice contained in this report.

We have prepared this report in accordance with the brief as provided and our terms of engagement. The information contained in this report has been prepared by Chester Consultants at the request of Realm Property Group Limited and is exclusively for its client use and reliance. It is not possible to make a proper assessment of this assessment without a clear understanding of the terms of engagement under which it has been prepared, including the scope of the instructions and directions given to and the assumptions made by Chester Consultants. The assessment will not address issues which would need to be considered for another party if that party's particular circumstances, requirements and experience were known and, further, may make assumptions about matters of which a third party is not aware. No responsibility or liability to any third party is accepted for any loss or damage whatsoever arising out of the use of or reliance on this assessment by any third party.

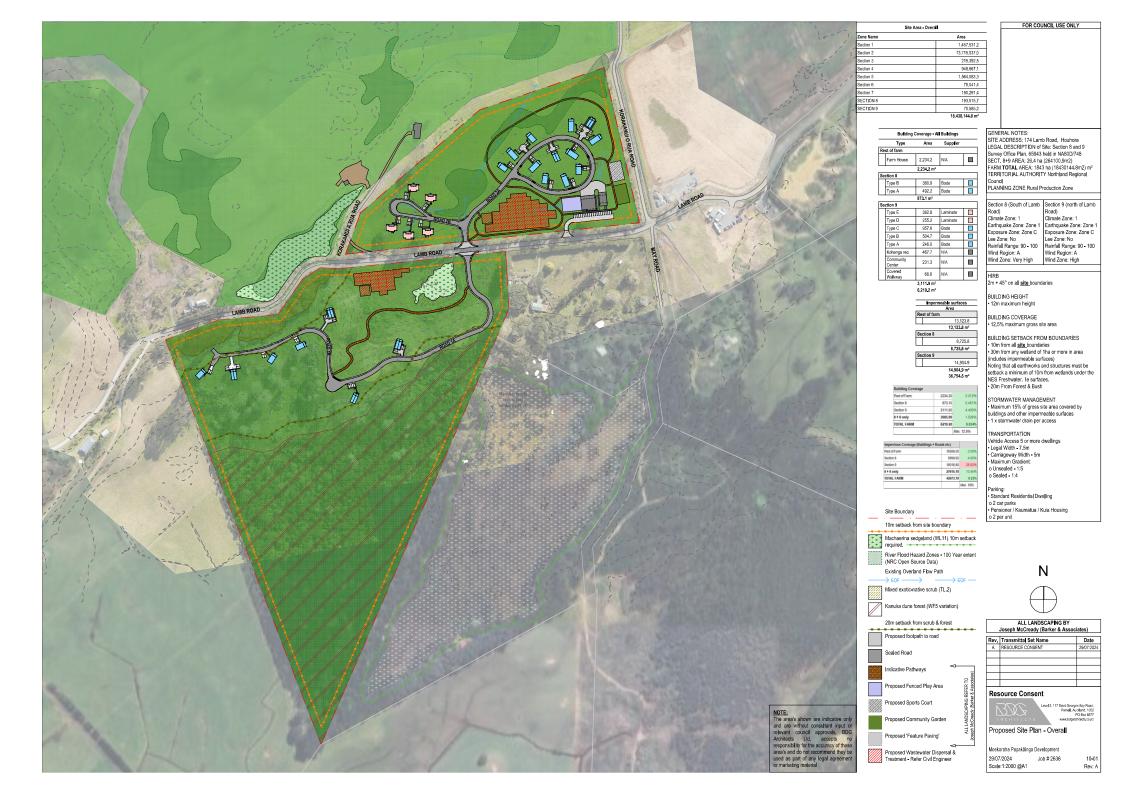
The assessment is also based on information that has been provided to Chester Consultants from other sources or by other parties. The assessment has been prepared strictly on the basis that the information that has been provided is accurate, completed, and adequate. To the extent that any information is inaccurate, incomplete or inadequate, Chester takes no responsibility and disclaims all liability whatsoever for any loss or damage that results from any conclusions based on information that has been provided to Chester Consultants.



12 Appendices

Appendix A – Architectural Site Plan by BDG





Appendix B – Chester Civil Design Drawings



		DEVICION DATE	29/07/2024					
SHEET	TITLE	REVISION DATE	REVISIOI	NI .				
001	DRAWING SCHEDULE							
			0					
002	NOTES AND ABBREVIATIONS		0					
100	EXISTING SITE PLAN		0					
110	PROPOSED SITE PLAN		0					
200	EARTHWORKS PLAN		0					
210	EROSION AND SEDIMENT CONTROL PLAN		0					
420	STORMWATER LAYOUT PLAN - PRIVATE NORTH		0					
421	STORMWATER LAYOUT PLAN - PRIVATE SOUTH		0					
520	WASTEWATER LAYOUT PLAN - PRIVATE NORTH		0					
521	WASTEWATER LAYOUT PLAN - PRIVATE SOUTH		0					
600	WATER SUPPLY LAYOUT PLAN - NORTH		0					
601	WATER SUPPLY LAYOUT PLAN - SOUTH		0					
700	ROAD LAYOUT PLAN - ROAD 1A		0					
701	ROAD LAYOUT PLAN - ROAD 1B		0					
702	ROAD LAYOUT PLAN - ROAD 2A AND COMMUNITY CENTRE		0					
703	ROAD LAYOUT PLAN - ROAD 2B		0					
720	TYPICAL PAVEMENT CROSS SECTIONS - SHEET 1		0					
721	TYPICAL PAVEMENT CROSS SECTIONS - SHEET 2		0					

SCHEDULE LEGEND	
ORIGINAL ISSUE	0
NOT REVISED	
REVISED	1
NOT INCLUDED IN SET	-
DELETED FROM SET	TITLE

CIVIL DESIGN MOEKORAHA PAPAKAINGA DEVELOPMENT 174 LAMB ROAD, HOUHORA

0 29/07/24 FOR CONSENT Rev Date Amendments	PL By	Date: 29/07/2024	Drawing Title	: DRAWING SCHEDULE	lssue:	FOR CONSENT	www.chester.co.nz
		Checker: N JULL	Address:	174 LAMB ROAD, PUKENUI	Projec	t: 15657	LAND DEVELOPMENT & INFRASTRUCTURE ENGINEERING SURVEYING PLANNING
		Designer: P LIEBENBERG	Client:	REALM PROPERTY GROUP LTD	Scale:	NTS	CHESTER
		Drafter: P LIEBENBERG	Job Title:	PROPOSED DEVELOPMENT AT 174 LAMB ROAD, PUKENUI	Drawin	g: 001 Rev: 0	CLICCTOD

GENERAL ABBREVIATIONS

EXISTING

PROPOSED

BOUNDARY

REDUCED LEVEL

RETAINING WALL

BOTTOM OF WALL

TOP OF WALL

GEOMETRY ABBREVIATIONS

LEFT

RIGHT

CENTRE LINE

HIGH POINT

CURVE COEFFICIENT

0 29/07/24 FOR CONSENT

Rev Date Amendments

FINISH FLOOR LEVEL

GARAGE FLOOR LEVEL

ΕX

PROP

BNDY

RL

FFL

GFL

RW

TOW

BOW

CL

- 2. CONCRETE CONSTRUCTION IS TO BE IN ACCORDANCE WITH NZS 3109 AND NZS 3114.

 (NZS 3109 CONCRETE CONSTRUCTION)

 (NZS 3114 SPECIFICATIONS FOR CONCRETE SURFACE FINISHES)
- DIMENSIONS ARE IN METRES UNLESS OTHERWISE NOTED.
- 4. SURFACE FINISH OF CONCRETE PAVEMENT TO BE US PER NZS 3114.
- CONTRACTION (SAWCUT) JOINTS AT 4m INTERVALS. JOINT DEPTH TO BE 1/4 OF CONCRETE DEPTH.

UNDERGROUND UTILITIES NOTES

- UNDERGROUND UTILITIES SHOWN IN PLANS ARE BASED ON VARIOUS SOURCES OF DIFFERING QUALITY AND SHALL BE CONSIDERED INDICATIVE.
- 2. CONTRACTOR IS RESPONSIBLE FOR LOCATING
 UNDERGROUND UTILITIES TO CONFIRM LOCATIONS OF
 SHOWN UTILITIES OR IDENTIFY UTILITIES NOT SHOWN
 ON PLANS ALONG PATHS OF EXCAVATION
- IF UTILITY CLASHES ARE FOUND, THE CONTRACTOR SHALL NOTIFY THE ENGINEER.

SEDIMENT AND EROSION CONTROL NOTES

- ALL WORKS ARE TO BE IN ACCORDANCE WITH AUCKLAND COUNCIL GUIDANCE DOCUMENT 2016/05 (GD05), EROSION AND SEDIMENT CONTROL GUIDE.
- 2. THESE PLANS DETAIL THE GENERAL SEDIMENT AND EROSION CONTROL MEASURES. ACTUAL CONTROLS ARE TO BE THE RESPONSIBILITY OF THE CONTRACTOR AND ARE TO BE ADAPTED TO SUIT THE CURRENT STAGE OF WORKS.

PRIVATE WASTEWATER NOTES

- PRIVATE WASTEWATER TO COMPLY WITH NEW ZEALAND BUILDING CODE G13-FOUL WATER AND, G13/AS2
- 2. DRAINAGE PIPES TO BE 100mm ϕ uPVC SN8 UNLESS OTHERWISE NOTED.
- MINIMUM GRADIENTS FOR 100mmø DRAINS TO BE NO LESS THAN 1 IN 120 (0.8%).
- 4. INSPECTION POINTS TO BE LOCATED AT CHANGES IN DIRECTION GREATER THAN 45° UNLESS OTHERWISE NOTED
- 5. INSPECTION POINTS TO BE LOCATED AT JUNCTIONS OF DRAINS, UNLESS DRAIN SERVES A GULLY TRAP LESS THAN 2m AWAY, OR UNLESS OTHERWISE NOTED.
- 6. DRAINS LAID UNDER BUILDINGS SHALL BE RUN IN A STRAIGHT LINE FROM ONE SIDE TO THE OTHER WITH A RODDING POINT LOCATED WITHIN 2 METRES FROM THE DOWNSTREAM EXTERIOR BUILDING FACE.
- WHERE TRENCH GRADIENTS ARE 1 IN 8 (12.5%0 OR STEEPER, ANTI-SCOUR BLOCKS SHALL BE REQUIRED.
- 8. TRENCHES SHALL BE OPEN FOR NO MORE THAN 48
 HOURS WITHOUT SPECIFIC APPROVAL FROM
 FNGINFFR
- TRENCHES SHALL REMAIN OUTSIDE THE ZONE-OF-INFLUENCE OF BUILDING FOUNDATIONS AS DEFINED BY NZBC EA/AS1, SECTION 3.9.7.

PRIVATE STORMWATER NOTES

- PRIVATE STORMWATER TO COMPLY WITH NEW ZEALAND BUILDING CODE E1-SURFACE WATER AND, F1/AS1
- DRAINAGE PIPES TO BE 100mmø uPVC SN8 UNLESS OTHERWISE NOTED.
- MINIMUM GRADIENTS FOR 100mm DRAINS TO BE NO LESS THAN 1 IN 120 (0.8%).
- 4. TYPE 2 CATCHPIT LEADS TO BE 150mmø uPVC SN8
- UNLESS OTHERWISE NOTED.

 3. MINIMUM GRADIENTS FOR 150mmø DRAINS TO BE NO
- LESS THAN 1 IN 200 (0.5%).

 4. SUB-SOIL DRAINAGE, INCLUDING RETAINING WALL

 DRAINAGE, TO BE 110 pp. 4 NOVACCII, UNI ESS
- DRAINAGE, TO BE 110mmø NOVACOIL UNLESS
 OTHERWISE NOTED.
- 5. SUB-SOIL DRAINS TO DISCHARGE TO PRIVATE CATCHPITS WITHIN THE SITE BOUNDARY.
- INSPECTION POINTS TO BE LOCATED AT CHANGES IN DIRECTION GREATER THAN 45° UNLESS OTHERWISE NOTED.
- 7. INSPECTION POINTS TO BE LOCATED AT JUNCTIONS OF DRAINS, UNLESS DRAIN SERVES A SINGLE DOWNPIPE LESS THAN 2m AWAY, OR UNLESS OTHERWISE NOTED.
- 8. INSPECTION CHAMBERS OR NON-ACCESS CHAMBERS TO BE LOCATED AT CHANGES TO BOTH GRADIENT AND DIRECTION OCCUR AND WHERE EITHER IS GREATER THAN 22.5° UNLESS OTHERWISE NOTED.
- DRAINS LAID UNDER BUILDINGS SHALL BE RUN IN A STRAIGHT LINE FROM ONE SIDE TO THE OTHER WITH A RODDING POINT LOCATED WITHIN 2 METRES FROM EXTERIOR BUILDING FACE.
- WHERE TRENCH GRADIENTS ARE 1 IN 8 (12.5%) OR STEEPER, ANTI-SCOUR BLOCKS SHALL BE REQUIRED.
- 11. TRENCHES SHALL BE OPEN FOR NO MORE THAN 48
 HOURS WITHOUT SPECIFIC APPROVAL FROM
 ENGINEER.
- 12. TRENCHES SHALL REMAIN OUTSIDE THE ZONE-OF-INFLUENCE OF BUILDING FOUNDATIONS AS DEFINED BY NZBC EA/AS1, SECTION 3.9.7.
- PRIVATE DRAIN OUTFALLS MAY REQUIRE A RESOURCE CONSENT.

GENERAL NOTES

- ALL DIMENSIONS AND LEVELS ARE TO BE CHECKED AGAINST THE SITE DRAWINGS PRIOR TO COMMENCING WORK.
- 2. DIMENSIONS ARE IN METRES UNLESS OTHERWISE NOTED.
- ANY VARIATIONS OR DISCREPANCIES ARE TO BE REFERRED TO CHESTER CONSULTANTS LTD FOR RESOLUTION.
- 4. ALL SERVICES ARE TO BE LOCATED AND FLAGGED PRIOR TO COMMENCING WORK ON SITE.
- WORKS TO BE IN ACCORDANCE WITH WSL STANDARDS, AUCKLAND COUNCIL STANDARDS, AND THE NEW ZEALAND BUILDING CODE.
- THE CONTRACTOR IS TO OBTAIN ALL NECESSARY CONSENTS AND PERMITS FOR WORKS ON, IN, AND AROUND EXISTING SERVICES, ASSETS, AND THE ROAD AND ROAD RESERVE.
- 7. ELECTRONIC FILES PROVIDED AS SUPPLEMENTAL INFORMATION TO DRAWINGS AND REPORTS. IF DISCREPANCIES ARE FOUND BETWEEN ELECTRONIC FILES AND DRAWINGS, CONTRACTOR TO NOTIFY ENGINEER. DRAWINGS SHALL TAKE PRECEDENT OVER ELECTRONIC FILES UNLESS OTHERWISE NOTED OR DIRECTED BY ENGINEER.

SURVEY NOTES

- EXISTING SITE BOUNDARIES HAVE BEEN CALCULATED FROM THE TITLE PLANS. DRAWING PROJECTION: NZGD2000 / MOUNT EDEN 2000 (EPSG:2105). NO SURVEYING HAS BEEN COMPLETED ON SITE.
- SHOWN CONTOURS BASED ON NRC 2018 LIDAR RETRIEVED FROM LINZ LAND ONLINE.

CONTRACTOR CONSENT NOTES

- IT IS THE CONTRACTOR'S RESPONSIBILITY TO BE FAMILIAR WITH THE RELEVANT STANDARDS, PROCESSES, AND APPROVALS REQUIRED TO EXECUTE WORK AS APPROVED BY RESOURCE CONSENT, BUILDING CONSENT, AND/OR ENGINEERING APPROVAL.
- 2. IT IS THE CONTRACTOR'S RESPONSIBILITY TO BE FAMILIAR WITH THE RELEVANT STANDARDS, PROCESSES, AND APPROVALS REQUIRED TO WORK ON OR IN CLOSE PROXIMITY TO PUBLIC AND PRIVATE UTILITIES.
- 7. NOTES RELATING TO SPECIFIC APPROVALS AND/OR CONSENTS WITHIN THESE PLANS, OR IN RELATED REPORTS PREPARED BY CHESTER, ARE NOT INCLUSIVE OF ALL APPROVALS AND/OR CONSENTS REQUIRED TO EXECUTE THE WORK.
- 11. IT IS THE CONTRACTOR'S RESPONSIBILITY TO INFORM THE ENGINEER IF THE CONTRACTOR HAS DETERMINED THAT THE WORK CAN NOT BE EXECUTED IN ACCORDANCE WITH THE APPLICABLE STANDARDS, APPROVALS, AND/OR CONSENTS.
- 12. CONTRACTOR TO SECURE APPROVAL WHEN EXECUTING WORK WITHIN THE ROAD CORRIDOR FROM THE TERRITORIAL AUTHORITY AND/OR THE ROAD CONTROLLING AUTHORITY.
- 13. CONTRACTOR TO SECURE APPROVAL WHEN WORKING IN CLOSE PROXIMITY TO PUBLIC STORMWATER, WASTEWATER, WATER SERVICE ASSETS FROM THE TERRITORIAL AUTHORITY AND/OR ASSET OWNER/OPERATOR.
- 14. CONTRACTOR TO SECURE APPROVAL WHEN WORKING ON OR IN CLOSE PROXIMITY TO ELECTRICAL POWER, TELECOMMUNICATIONS, FIBRE, NATURAL GAS OR OTHER SERVICES FROM THE SERVICE OWNER/OPERATOR.

LP LOW POINT CHCHAINAGE UTILITY ABBREVIATIONS UTILITY ABBREVIATIONS BOA BEGIN OF ALIGNMENT ۷C VITRIFIED CLAY SW STORMWATER EOA END OF ALIGNMENT WASTFWATER FW FARTHFNWARF WW ΒP **BEGIN POINT** ΕP PUB. PUBLIC CONC CONCRETE FND POINT PRIV. PRIVATE CLS CEMENT LINED STEEL MID MIDDLE POINT INSPECTION CHAMBER DI DUCTILE IRON PC POINT OF CURVATURE IC (675mmø AND LARGER) WS WATER SERVICE POINT OF COMPOUND PCC INSPECTION POINT CURVATURE S۷ SLUICE VALVE ΙP (100/150mmø) POINT OF REVERSE G۷ GATE VALVE PRC CP CATCH PIT CURVATURE FΗ FIRE HYDRANT PΤ POINT OF TANGENCY SP SPLAY PIT EC FND CAP I.P. INTERSECTION POINT LL LID LEVEL FΡ FLUSHING POINT BLS **BEGIN LONGSECTION** INV INVERT LEVEL I۷ ISOLATION VALVE END LONGSECTION REINFORCED CONCRETE ELS RCRR AΒ ANCHOR BLOCK VERTICAL POINT OF RUBBER RING JOINT VΡC Ε ELECTRICAL POWER CLn CURVATURE CLASS n CONCRETE G NATURAL GAS VERTICAL POINT OF PΕ POLYETHYLENE VPT **TANGENCY TELECOMMUNICATIONS** UNPLASTICIZED POLYVINYL Т uPVC BRK GRADE BREAK CHLORIDE CS COMBINED SERVICES

ASBESTOS CONCRETE

Drafter: P LIEBENBERG Job Title: PROPOSED DEVELOPMENT AT 174 LAMB ROAD, PUKENUI

Designer: P LIEBENBERG Client: REALM PROPERTY GROUP LTD

Checker: N JULL Address: 174 LAMB ROAD, PUKENUI

Date: 29/07/2024 Drawing Title: NOTES AND ABBREVIATIONS

Drawing: 002 Rev: 0

Scale: NTS

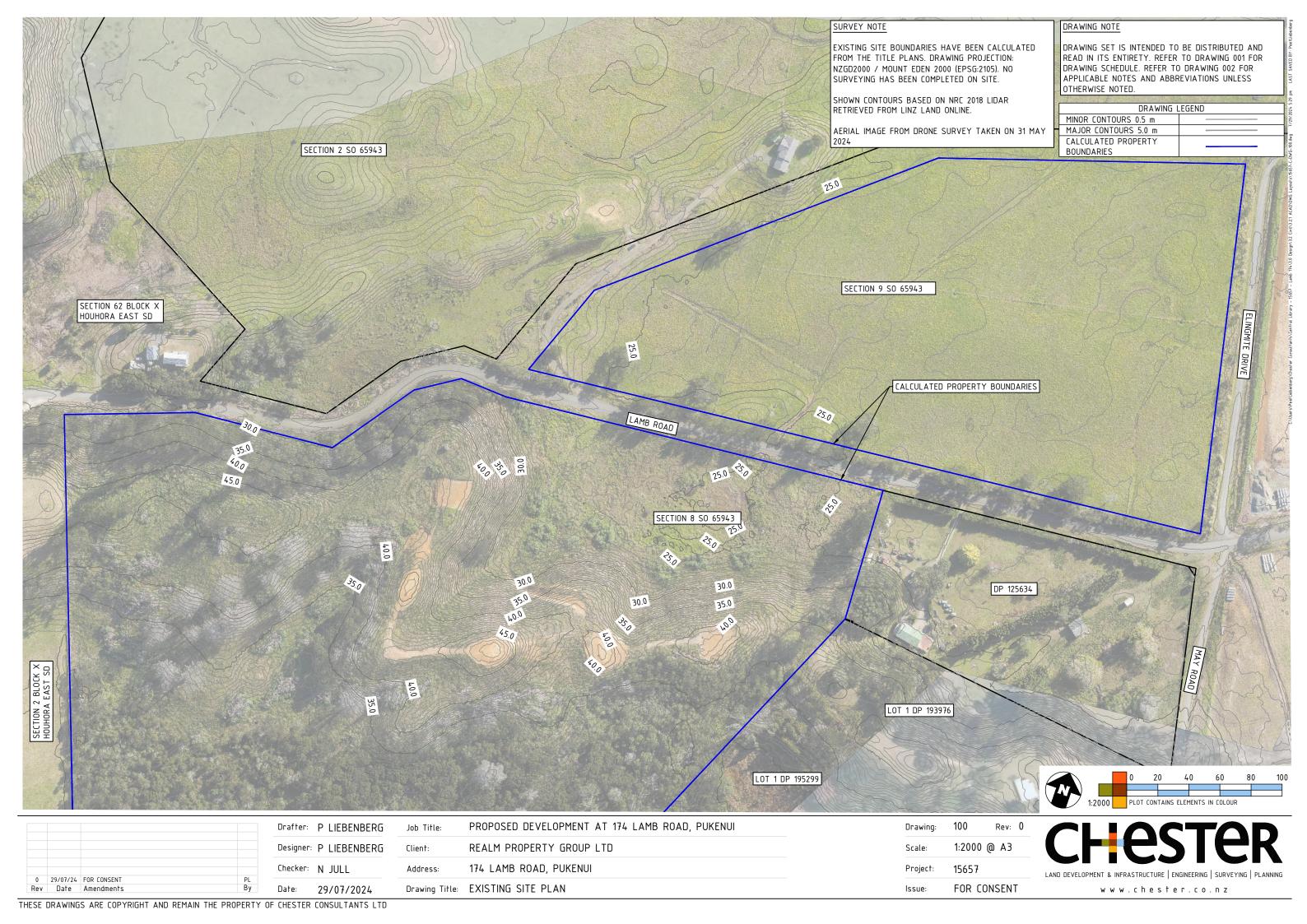
Project: 15657

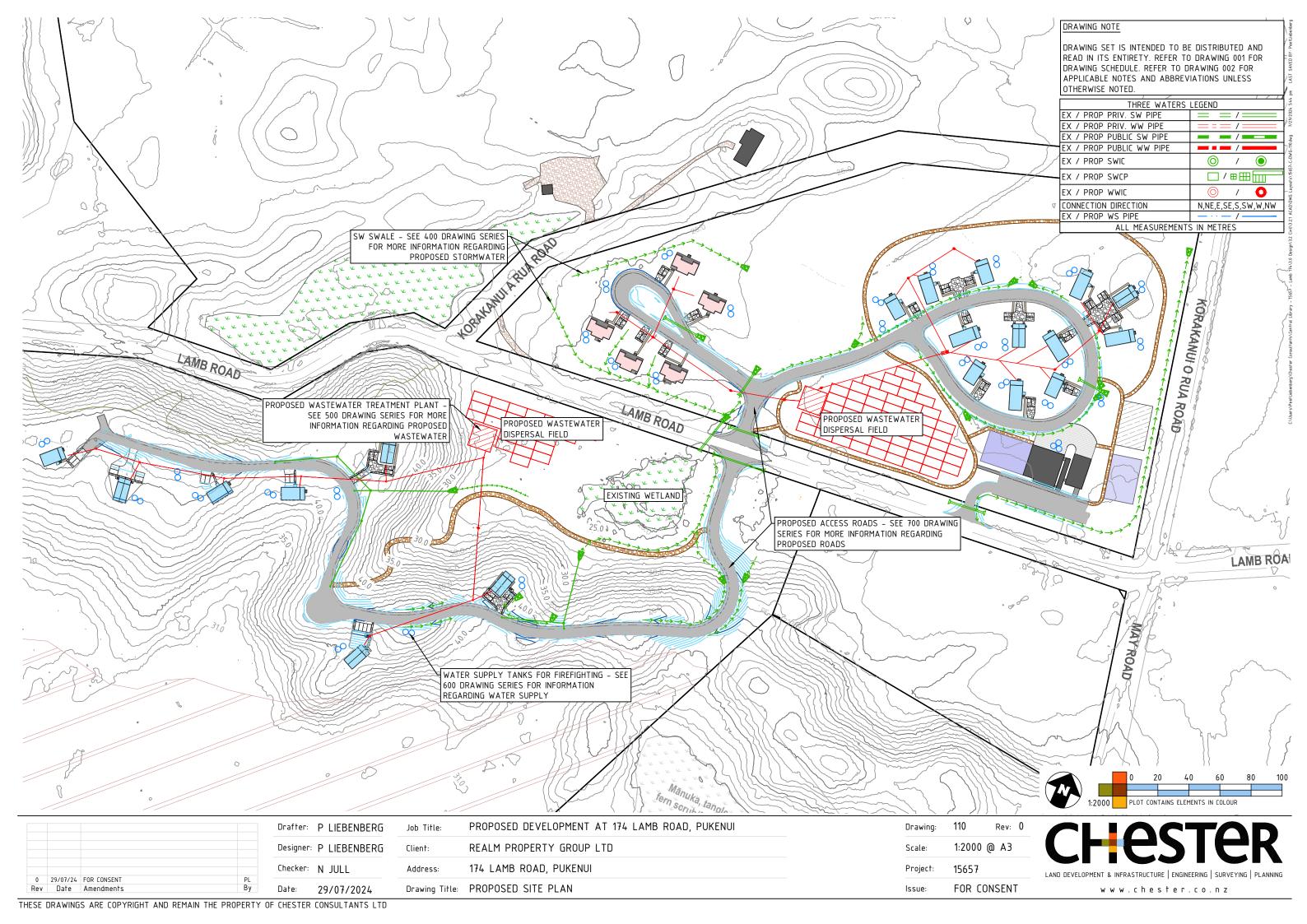
Issue: FOR CONSENT

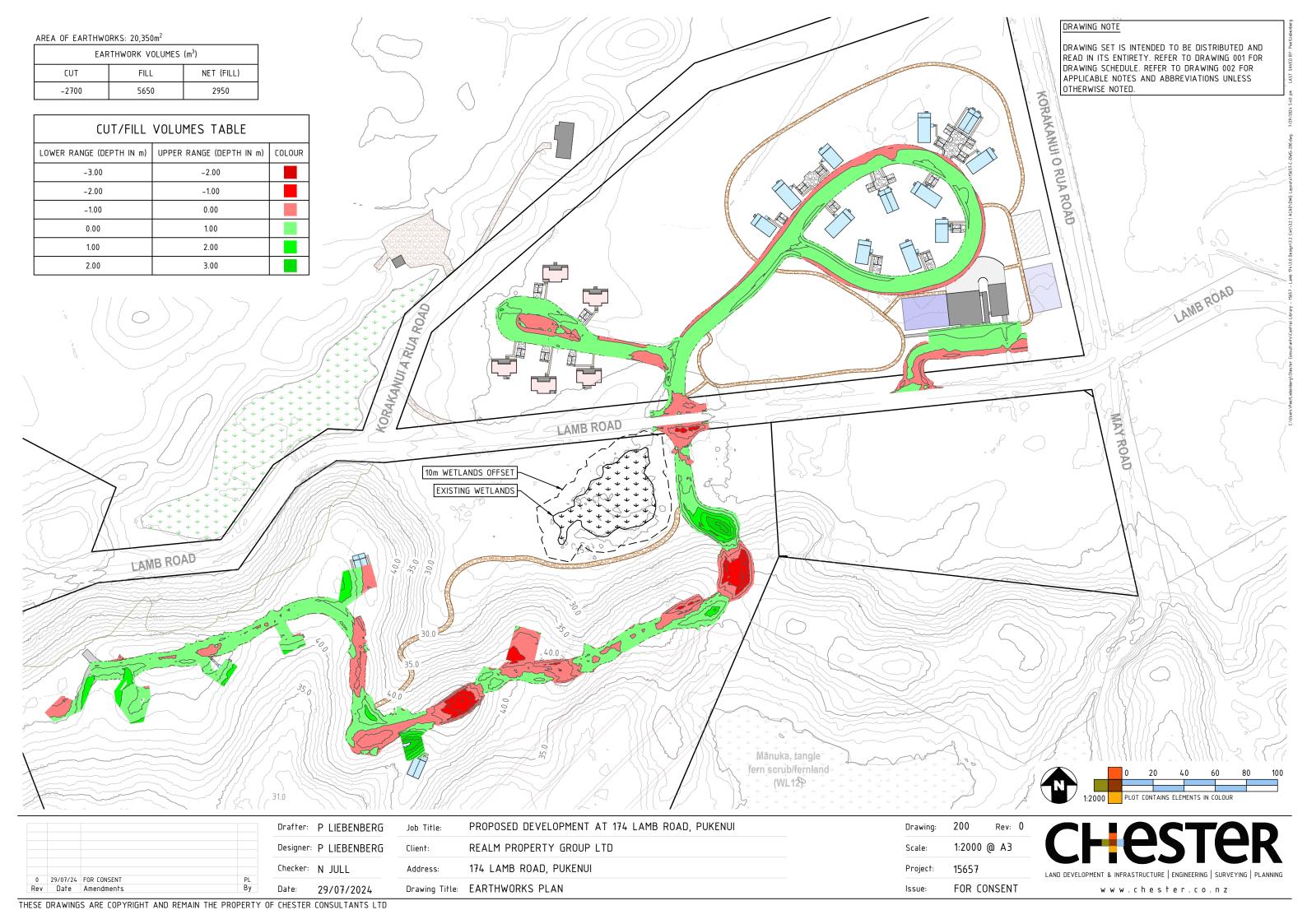


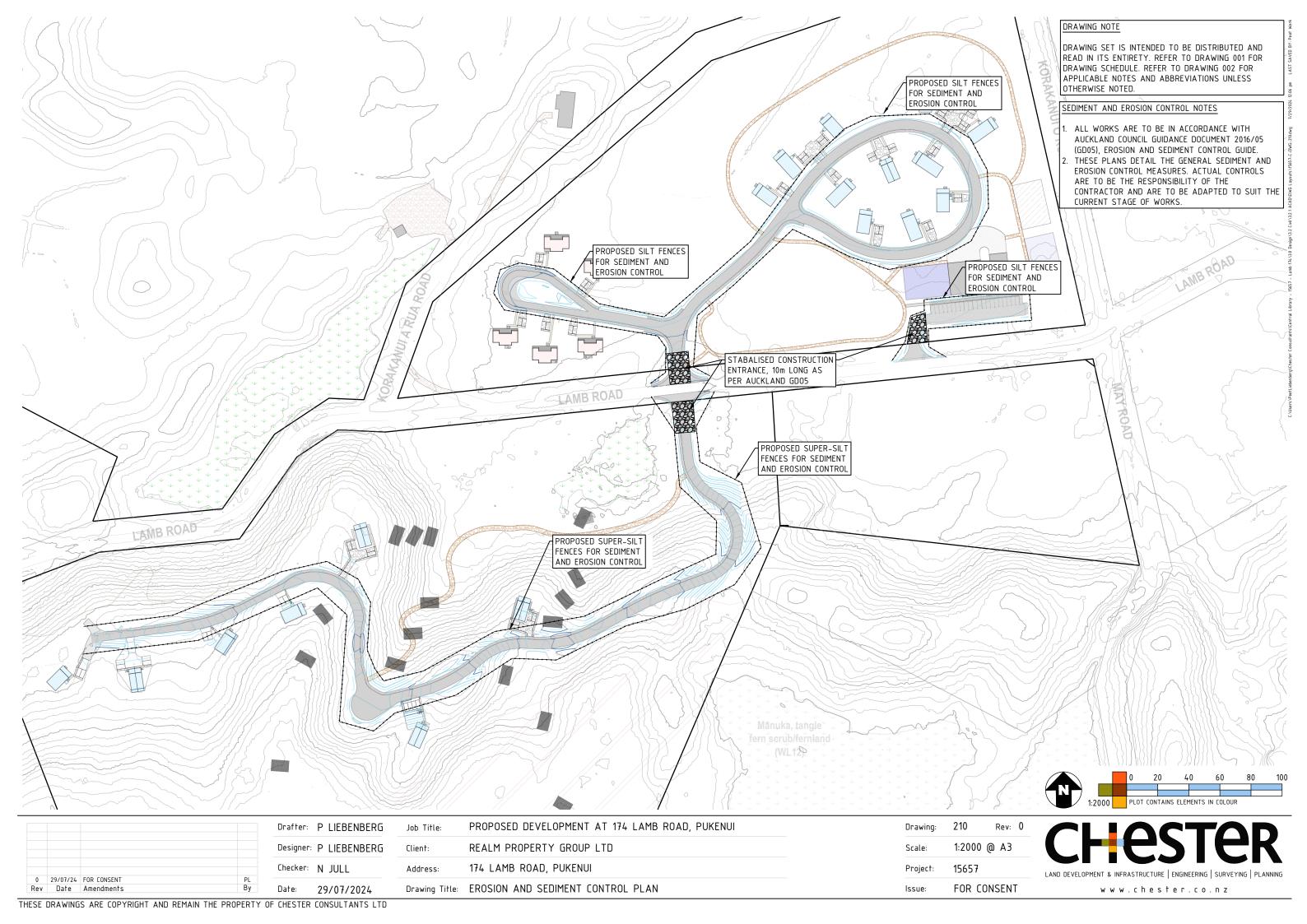
Ву

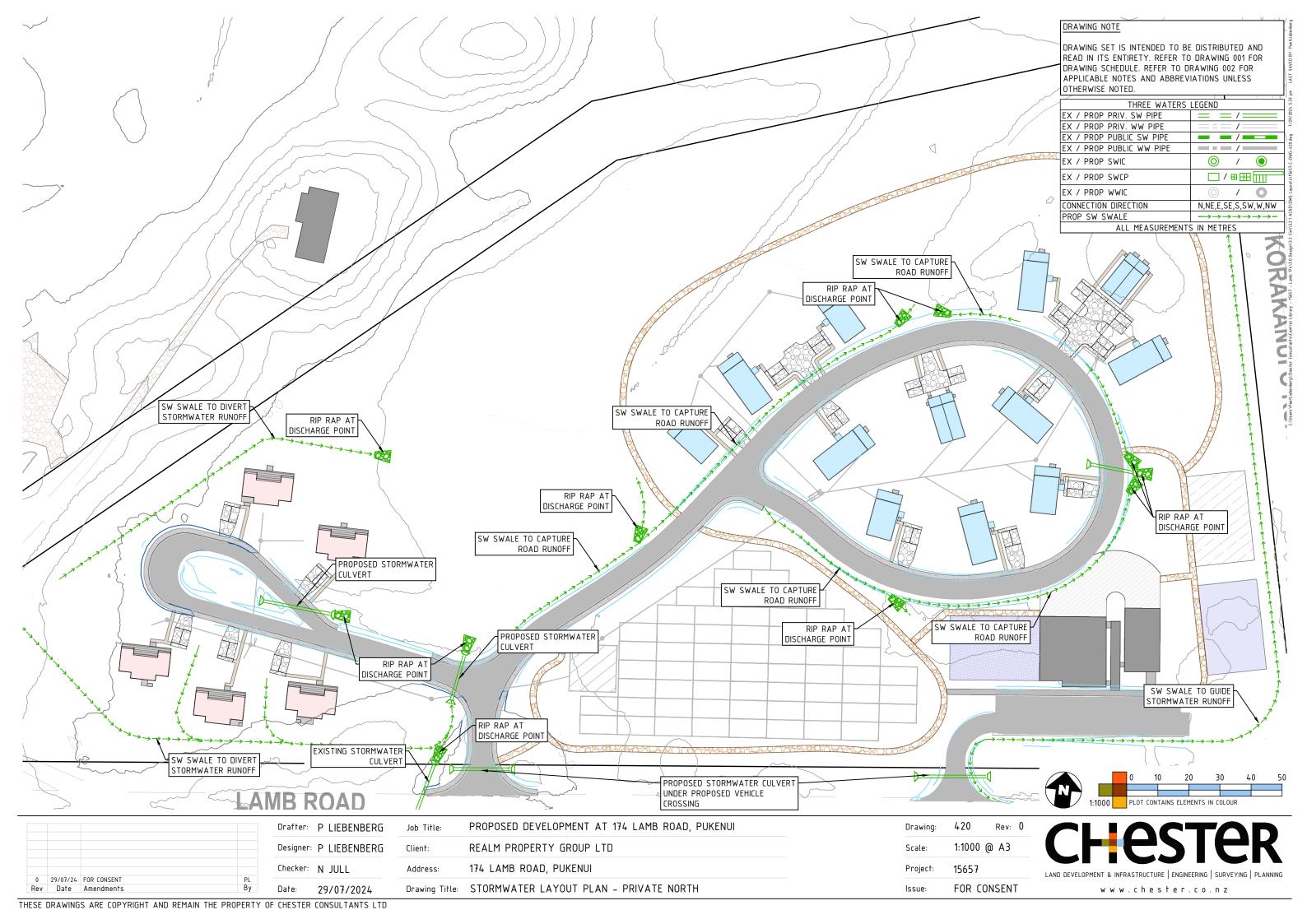
ΑC

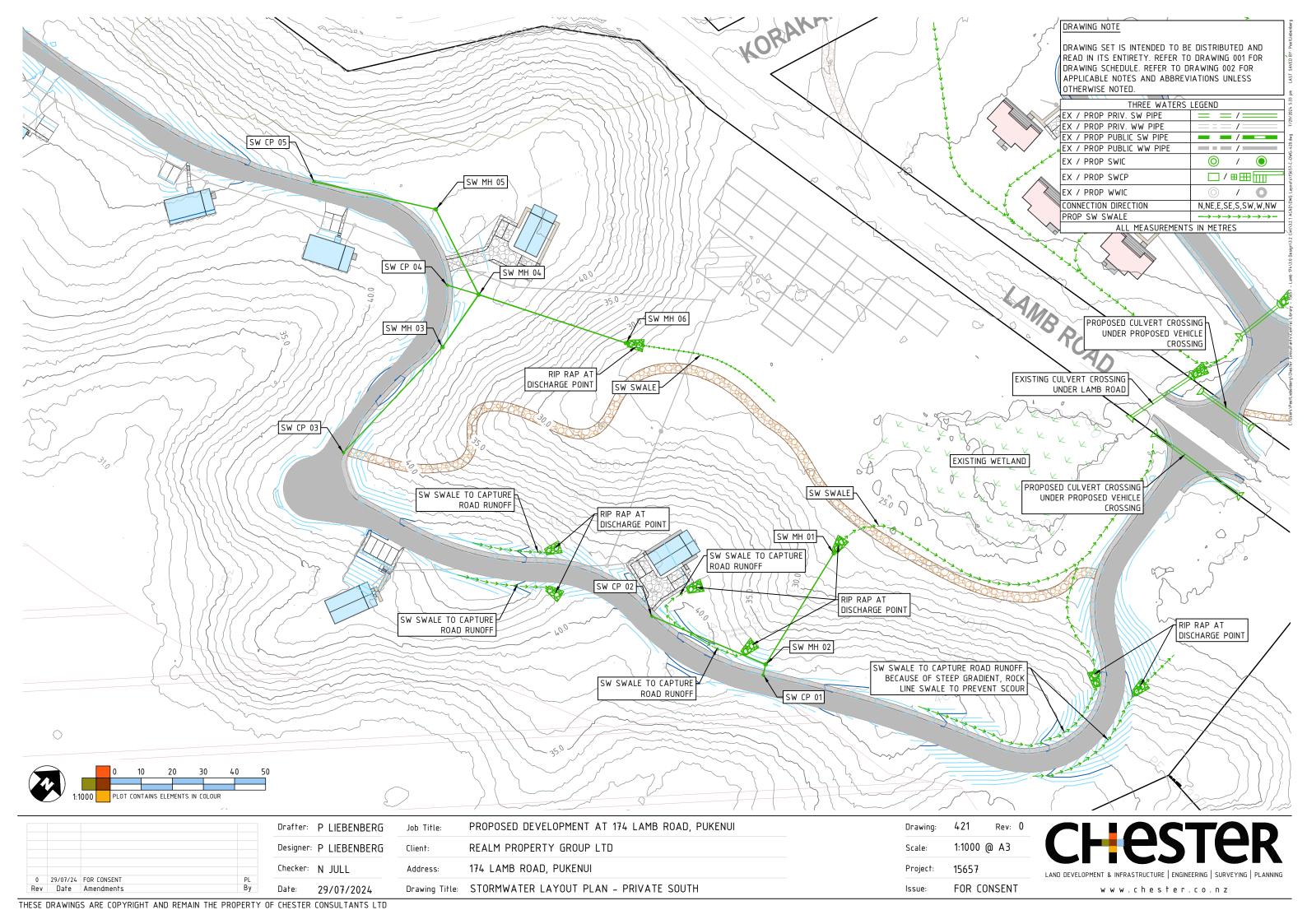


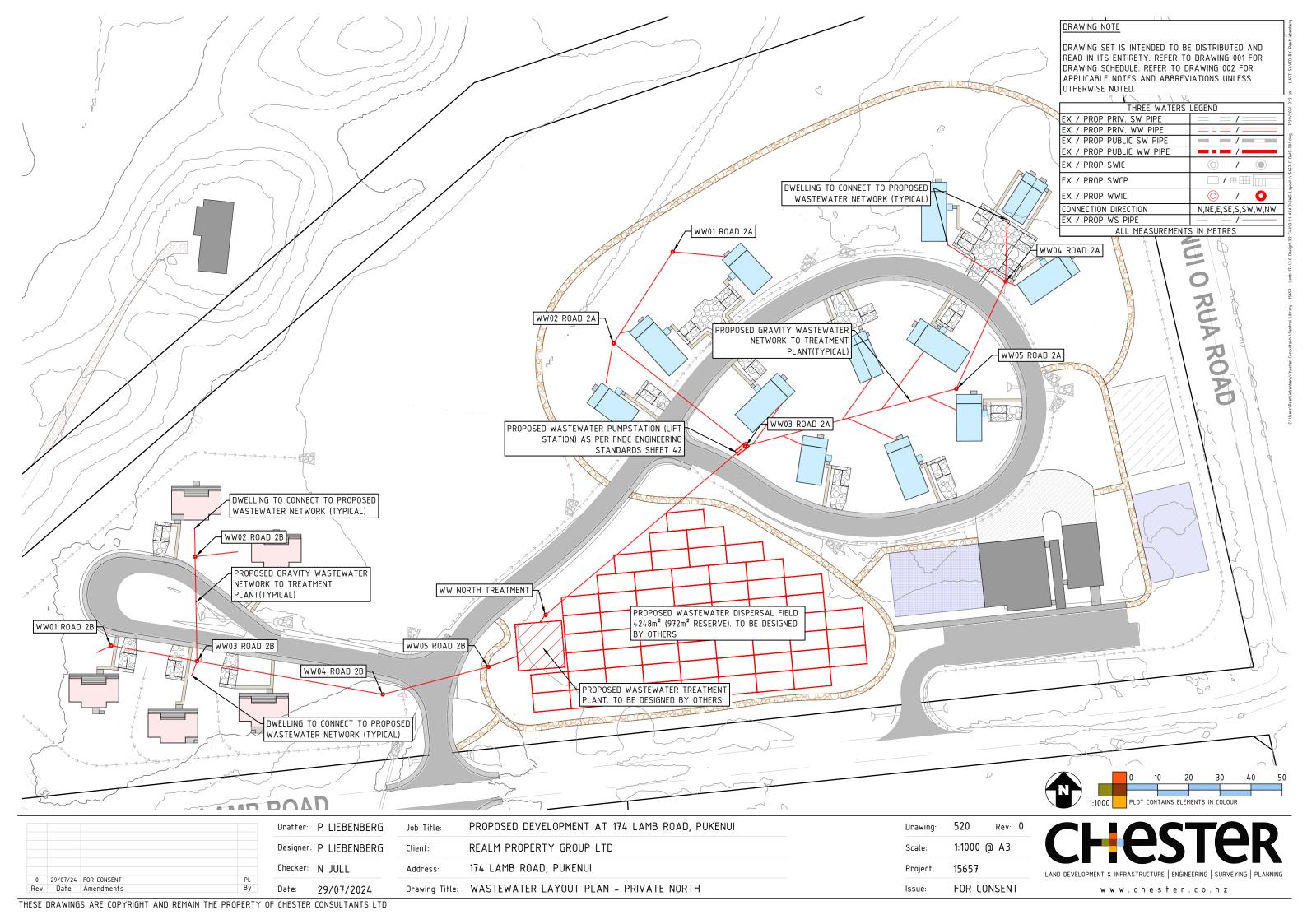


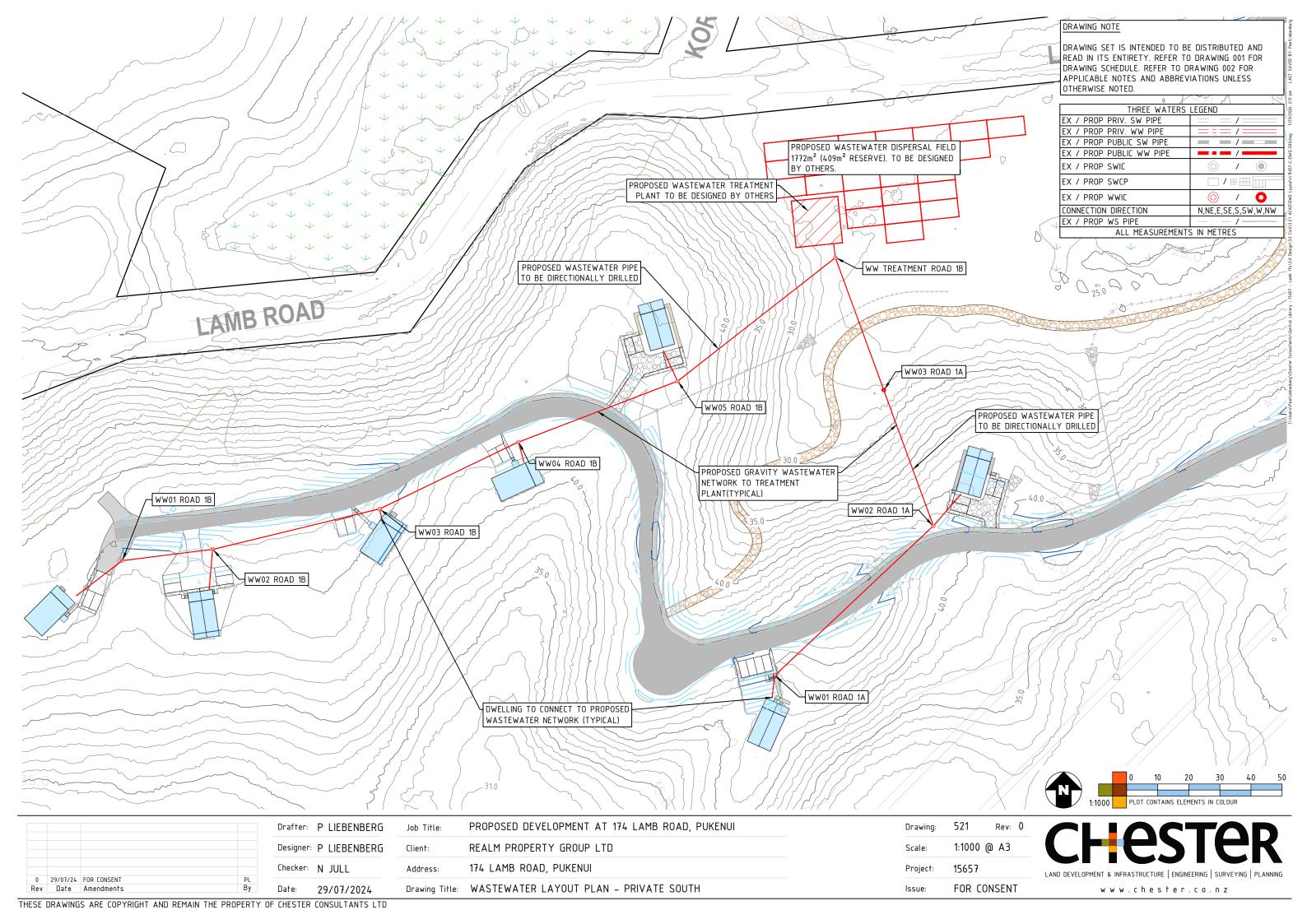


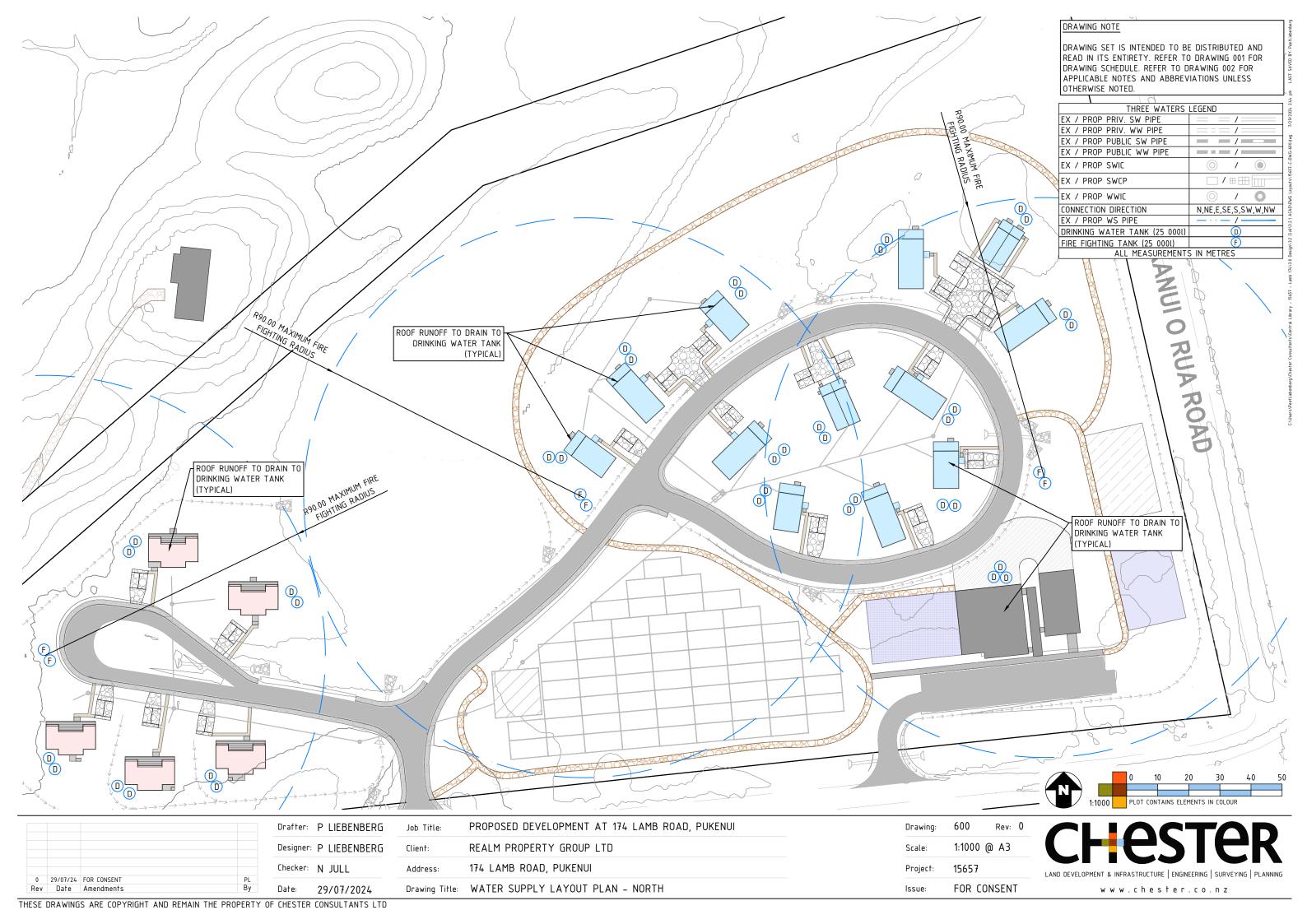


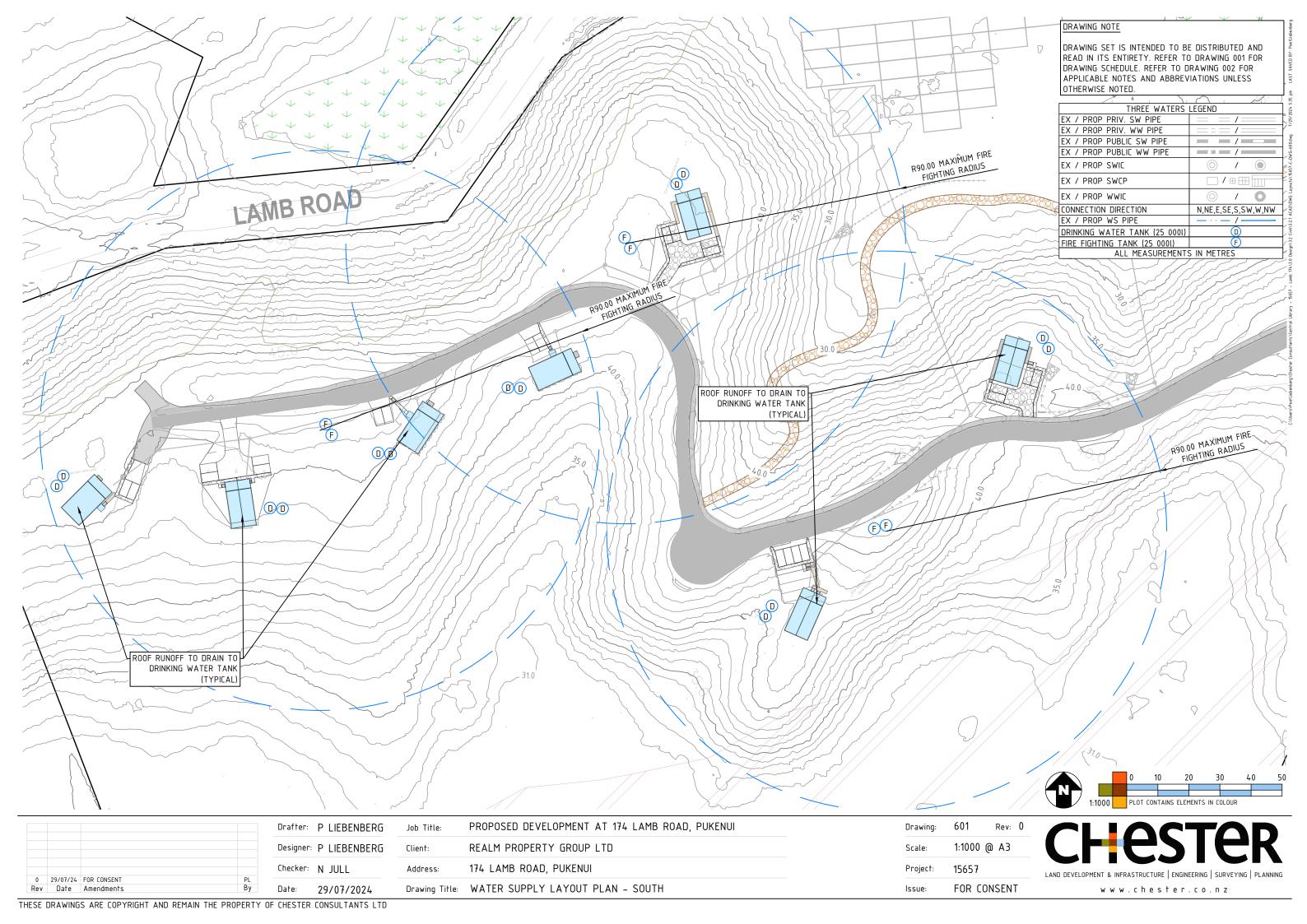


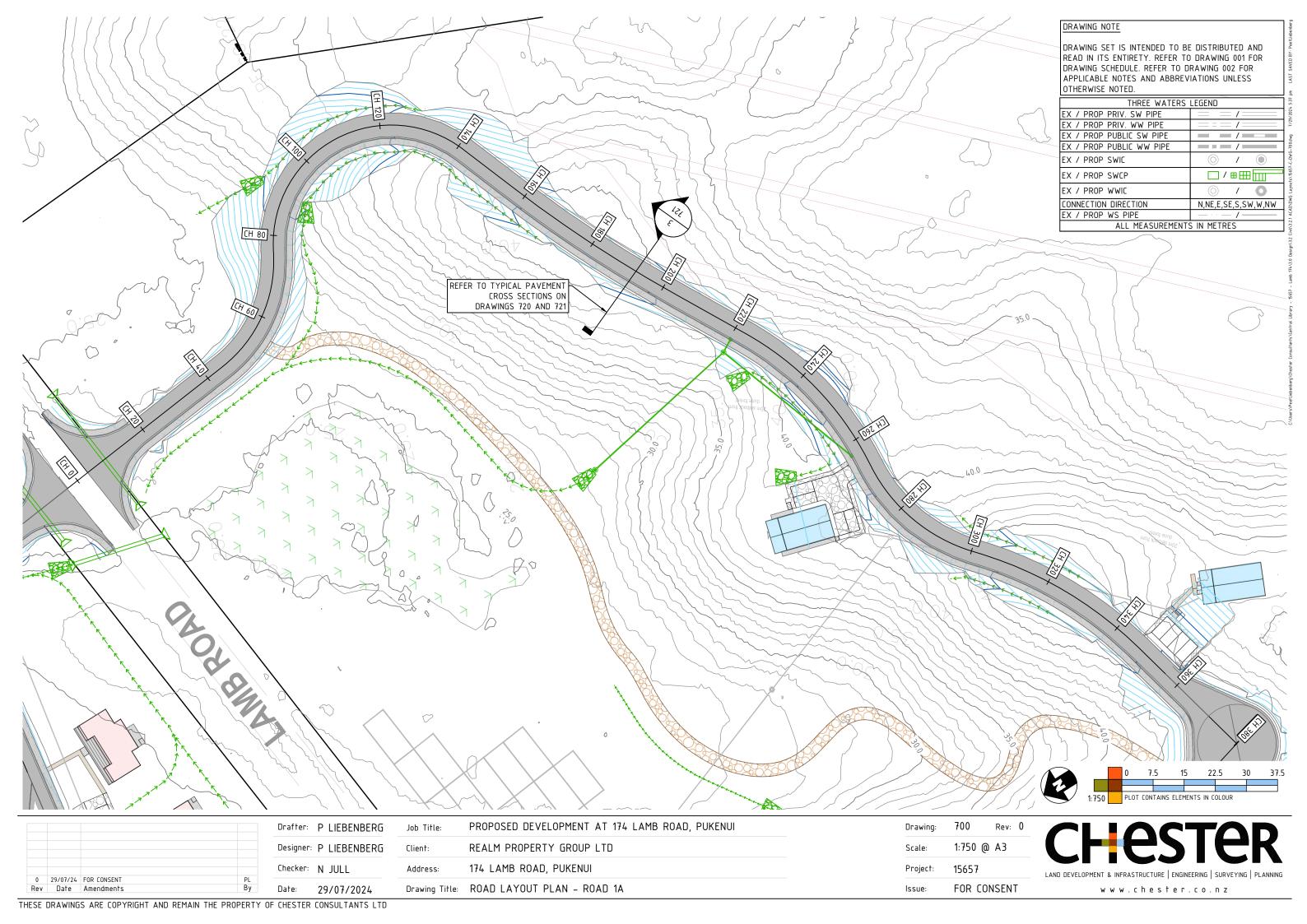


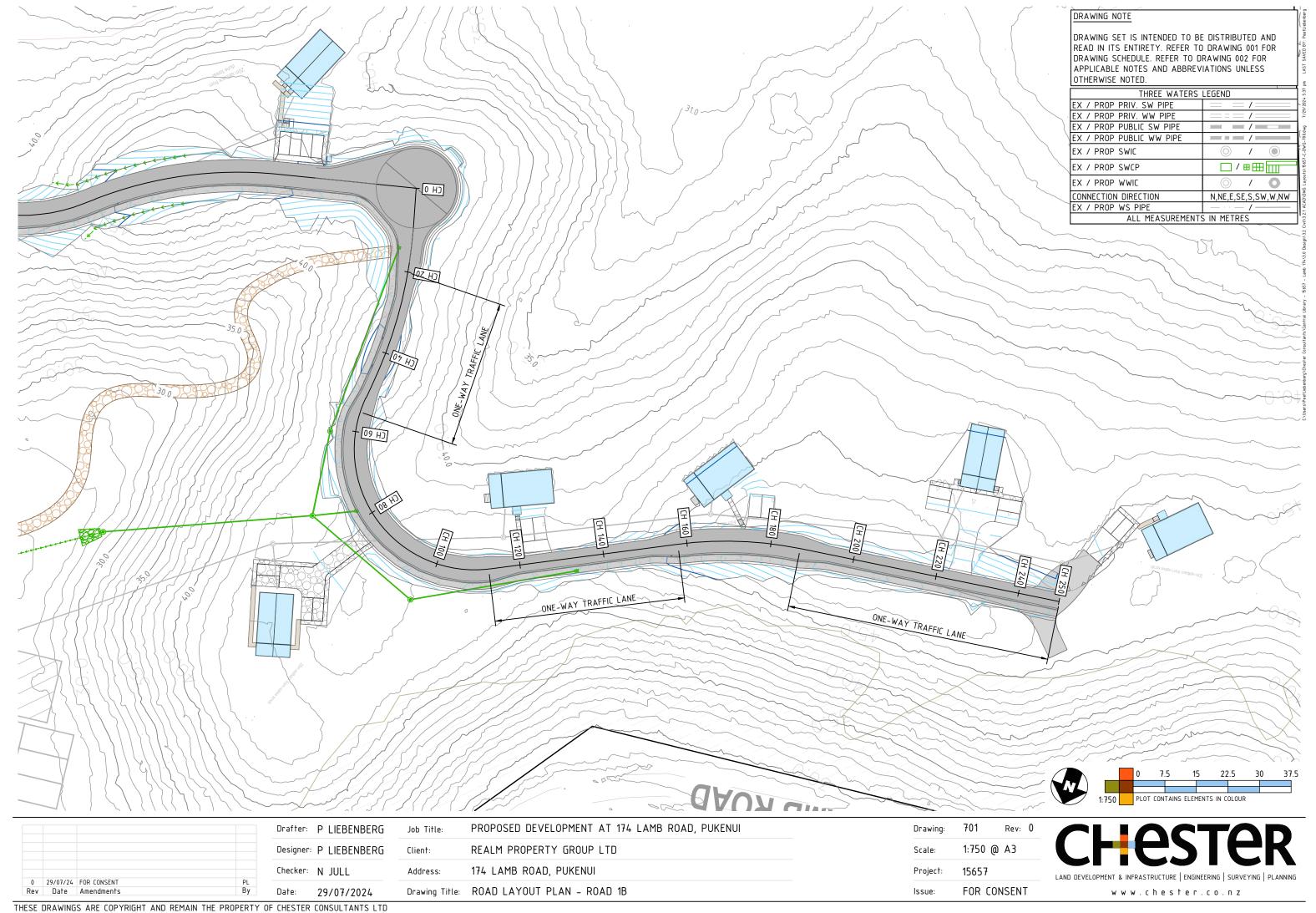


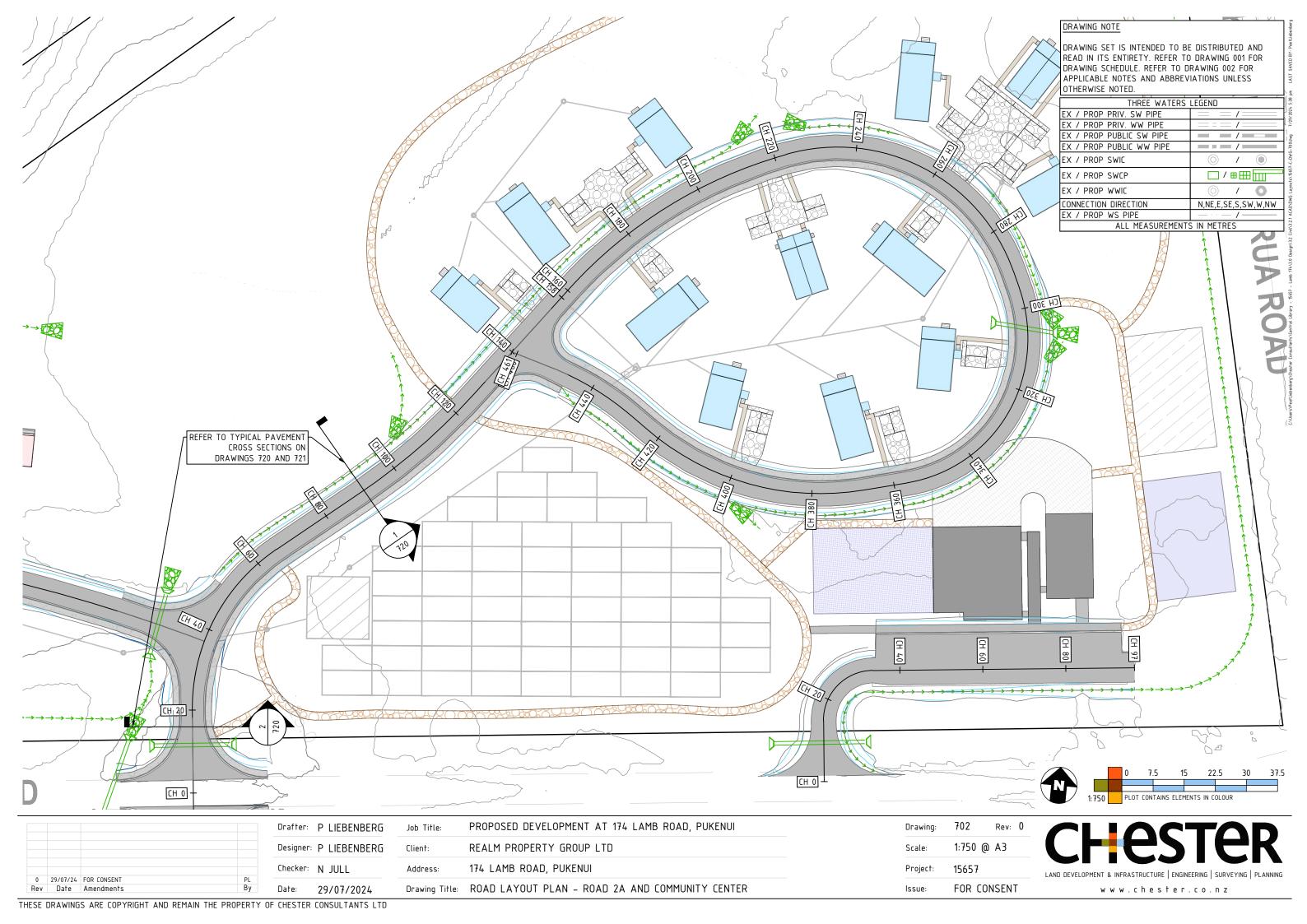


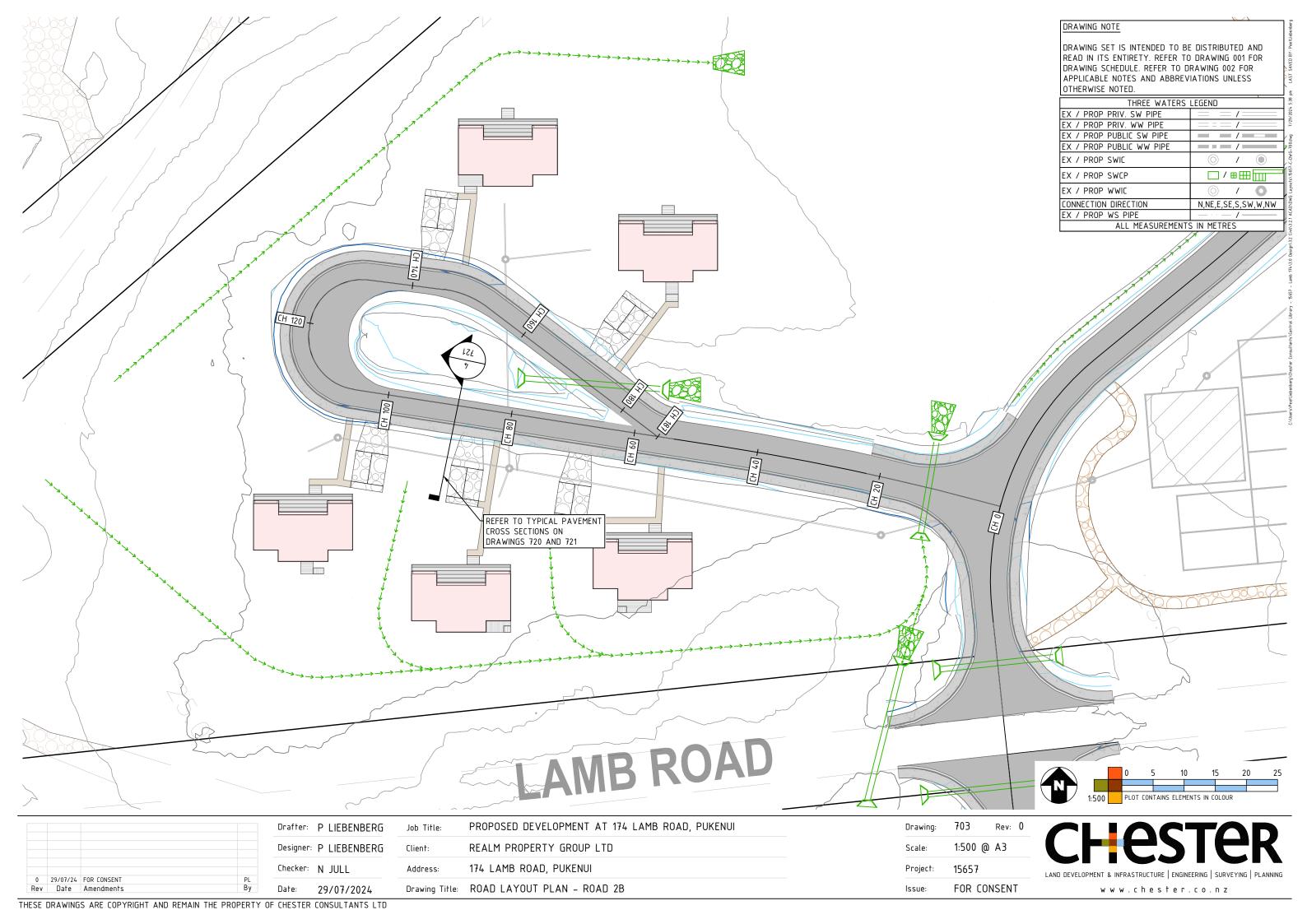


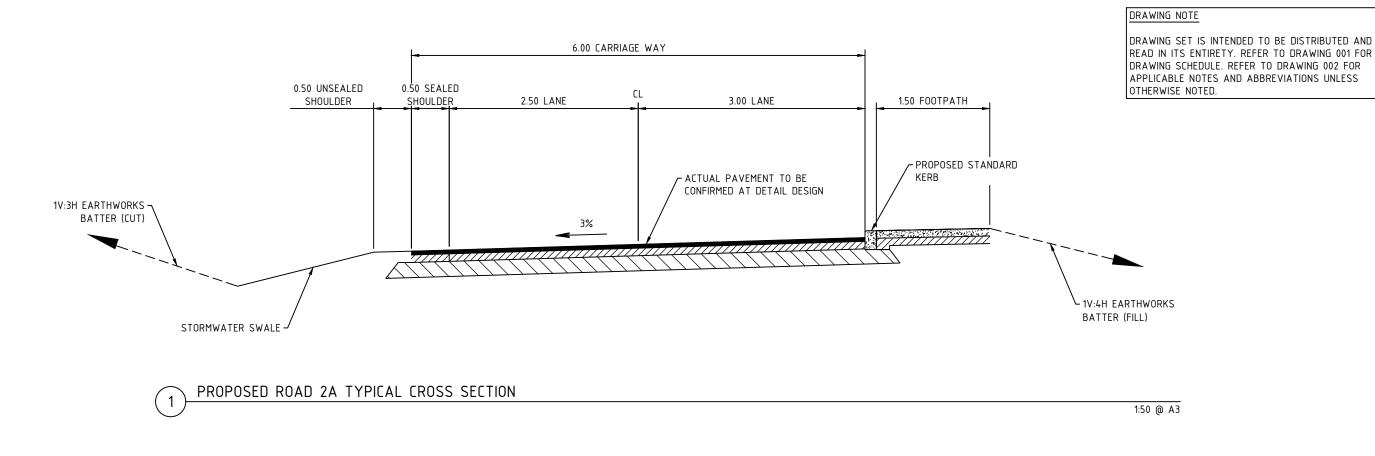


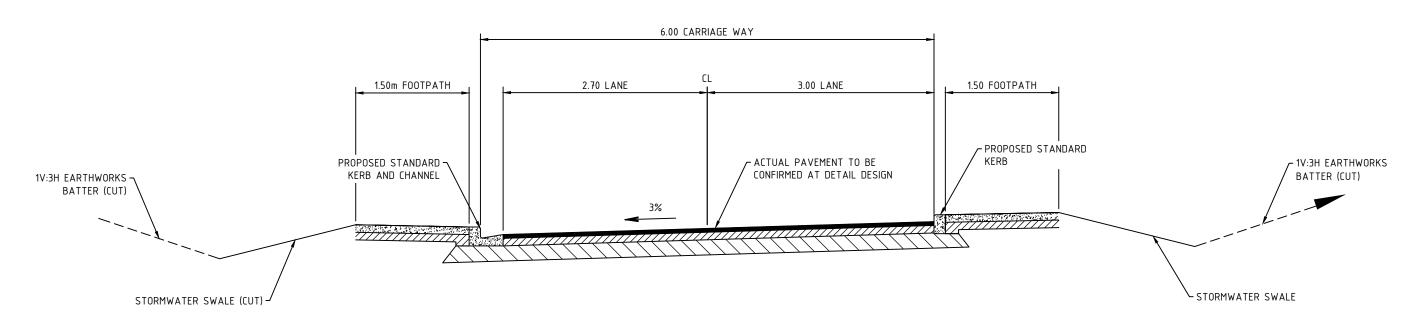












PROPOSED TYPICAL CROSS SECTION SIDEWALK BOTH SIDES

1:50 @ A3

				Drafter:	P LIEBENBERG	Job Title:	PROPOSED DEVELOPMENT AT 174 LAMB ROAD, PUKENUI
				Designer:	P LIEBENBERG	Client:	REALM PROPERTY GROUP LTD
				Checker:	N JULL	Address:	174 LAMB ROAD, PUKENUI
0	29/07/24	FOR CONSENT	PL				
Rev	Date	Amendments	Ву	Date:	29/07/2024	Drawing Title:	TYPICAL PAVEMENT CROSS SECTIONS - SHEET 1

 Drawing:
 720
 Rev: 0

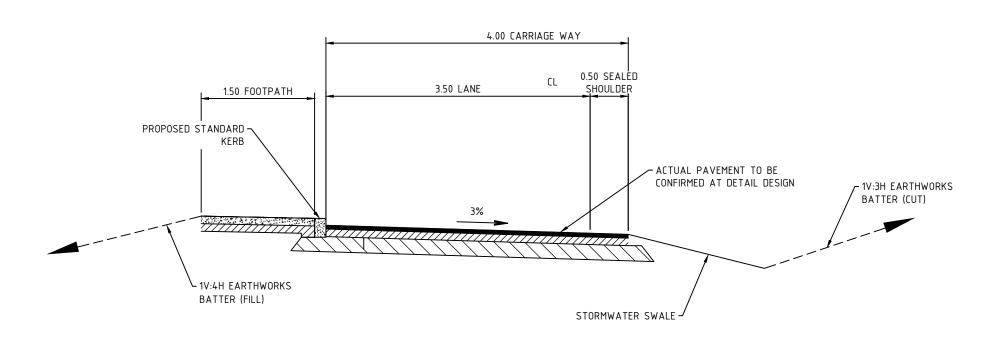
 Scale:
 1:50 @ A3

 Project:
 15657

 Issue:
 FOR CONSENT



DRAWING SET IS INTENDED TO BE DISTRIBUTED AND READ IN ITS ENTIRETY. REFER TO DRAWING 001 FOR DRAWING SCHEDULE. REFER TO DRAWING 002 FOR 6.00 CARRIAGE WAY APPLICABLE NOTES AND ABBREVIATIONS UNLESS OTHERWISE NOTED. 0.50 UNSEALED 0.50 SEALED 1.50m FOOTPATH 2.70 LANE 2.50 LANE SHOULDER SHOULDER PROPOSED STANDARD ¬ - ACTUAL PAVEMENT TO BE - 1V:3H EARTHWORKS KERB AND CHANNEL CONFIRMED AT DETAIL DESIGN 1V:3H EARTHWORKS -BATTER (CUT) BATTER (CUT) STORMWATER SWALE (CUT) -STORMWATER SWALE (CUT) PROPOSED ROAD 1 TYPICAL CROSS SECTION



PROPOSED ROAD 2B (ONE-WAY SECTION) TYPICAL CROSS SECTION

1:50 @ A3

DRAWING NOTE

1:50 @ A3

			Drafter:	P LIEBENBERG	Job Title:	PROPOSED DEVELOPMENT AT 174 LAMB ROAD, PUKENUI
			Designer:	P LIEBENBERG	Client:	REALM PROPERTY GROUP LTD
			Checker:	N JULL	Address:	174 LAMB ROAD, PUKENUI
0 Rev	FOR CONSENT Amendments	PL By	Date:	29/07/2024	Drawing Title:	TYPICAL PAVEMENT CROSS SECTIONS - SHEET 2

Drawing: 721 Rev: 0

Scale: 1:50 @ A3

Project: 15657

Issue: FOR CONSENT



Appendix D –Geotech Report By Soil and Rock Consultants







Preliminary Geotechnical Investigation for Proposed Development at

174 Lamb Road, Pukenui

Rev A

5 April 2024

Job No. NL230102











Auckland (09) 835 1740

Northland (09) 982 8053

Wellington (04) 896 0675

Christchurch (03) 352 4519

www.soilandrock.co.nz



PRELIMINARY GEOTECHNICAL INVESTIGATION FOR PROPOSED DEVELOPMENT AT 174 LAMB ROAD, PUKENUI

Job Number:	NL230102
Name of Project:	174 Lamb Road, Pukenui
Client:	Realm Property Group Ltd
Author:	Randy Lineses, Senior Geotechnical Engineer, MEngNZ
Reviewer & Authoriser:	Bruce Green, Principal Geotechnical Engineer, CMEngNZ, CPEng
Document Version:	A
Published:	5 April 2024
Author Signature:	
Reviewer & Authoriser Signature:	

COPYRIGHT:

The information presented in this document is the property of Soil & Rock Consultants. Use or copying of this document in whole or in part without the previous permission of Soil & Rock Consultants implies a breach of copyright.

Geotechnical Environmental Stormwater Hydrogeology

Table of Contents

Report	Summary	3
1.0	Introduction	
1.1	Limitations	2
2.0	Site Description	2
2.1	Proposed Development	6
3.0	Geology	7
4.0	Field Investigation	7
4.1	Subsurface Conditions	8
5.0	Sensitive Soils	11
6.0	Seismic Design Parameters	11
7.0	Slope Stability	11
8.0	Geotechnical Discussion	14
9.0	Preliminary Geotechnical Recommendations	15
9.1	Cuts and Fills	15
9.2	Retaining Structures	15
9.3	Pavements	16
9.4	Foundation Design Recommendations – Indicative	17
9.	4.1 Shallow Foundations	17
9.	4.2 Pile Foundations	17
10.0	Stormwater	18
11.0	On-site Wastewater Treatment and Dispersal	18
12.0	Site Constraints	19
13 0	Future Geotechnical Assessment	20

Appendices:

Appendix A: Drawings

Appendix B: Investigation Logs

Appendix C: Slope Stability Results

Report Summary

The following summarises the findings of this report however is not to be taken in isolation. It is a requirement that any user of this report review the document in its entirety, including all appendices.

Feature	Commentary
Proposal	Option 1, 2 & 3 sites are being considered for potential rural residential subdivision. The main consideration is the Option 1 site.
Fill	Not encountered within the test holes however was observed at the edges of the form platform in Option 1 Area.
Natural Soils	Loose to dense Karioitahi Group soils
Unduly Weak, Sensitive, or Compressible Soils	Not Encountered
Groundwater	Not encountered in most of the augerholes on the day of drilling, with the exception of AH20 (drilled within wetland area) where groundwater was measured at 1.1m bpgl.
Seismic Site Class	Site Class C
Slope Stability	Option 1 site - We consider the ridgeline area to be suitable for the future development from a land stability point of view. Option 2 site – The general area comprises gently sloping ground hence no undue global instability concern.
Preliminary Geotechnical Recommendations	Preliminary geotechnical recommendations (e.g. cuts, retaining, pavement, foundations) are provided in Section 9.0 of this report.
Site Constraint	Refer to Section 12.0 of this report.
Pavement	For preliminary design a CBR value of 3% or a modulus of subgrade reaction of 20kPa/mm are considered appropriate for flexible and rigid pavements respectively.

1.0 Introduction

Soil & Rock Consultants (S&RC) were engaged by Realm Property Group Ltd to carry out a geotechnical investigation relating to master planning of a proposed development at 174 Lamb Road, Pukenui.

The findings and recommendations of our investigation and analyses will be presented in a Preliminary Geotechnical Investigation Report suitable for master planning for the development as described in Section 2.0 of this report.

Further geotechnical assessment will be required following completion the final scheme prior to Resource Consent Application.

1.1 Limitations

This report has been prepared by Soil & Rock Consultants for the sole benefit of Realm Property Group Ltd (the client) with respect to 174 Lamb Road, Pukenui and the brief given to us. The data and/or opinions contained in this report may not be used in other contexts, for any other purpose or by any other party without our prior review and agreement. This report may only be read or transmitted in its entirety, including the appendices.

The preliminary recommendations given in this report are based on data obtained from discrete locations and soil conditions between locations are inferred only. Our geotechnical models are based on those actual and inferred conditions however variations between test locations may occur and Soil & Rock Consultants should be contacted in this event to confirm or modify the validity of this report.

2.0 Site Description

The subject properties are legally described as Section 8 SO 65943, Section 9 SO 65943, and Section 2 SO 65943 designated as Options 1, 2 and 3 respectively in Figure 1. Option 3 property is 174 Lamb Road, Pukenui.

Option 1 - The property is currently vacant. A broad ridgeline traversing from east to west in a zig-zag fashion is present within the northern section of the property. The ridge side slope inclinations range from 20° to 30°. A wetland is present within the northeastern section of the property, between the ridge and the road. The wetland appeared to be dry at time of our site visit. Land to the south of the ridgeline is covered with dense native bush.

The eastern section of the ridgeline has been cleared of vegetation and five building platforms and associated accessways have been created.

Option 2 - The property is currently vacant and used as grazing land. The ground surface is inclined generally less than 8° with isolated low/depressed areas. Some trees are present along and near the southern boundary. Multiple man-made open channels are present within the property, including a main drainage channel (approximately 1.5m deep near Lamb Road) entering the Option 2 area from across the road (wetland in Option 1 site) extending towards north-northeast beyond the property boundary. Refer to attached site plan for drainage alignment.

Option 3 - The Option 3 property is situated to the north and west of the Option 2 land. A dwelling serviced by a gravel driveway is present near the southeast boundary. Isolated elevated areas are present, including the location of the dwelling platform. The general area is currently used as grazing land. A wetland is present to the south of the property, adjacent to the road.

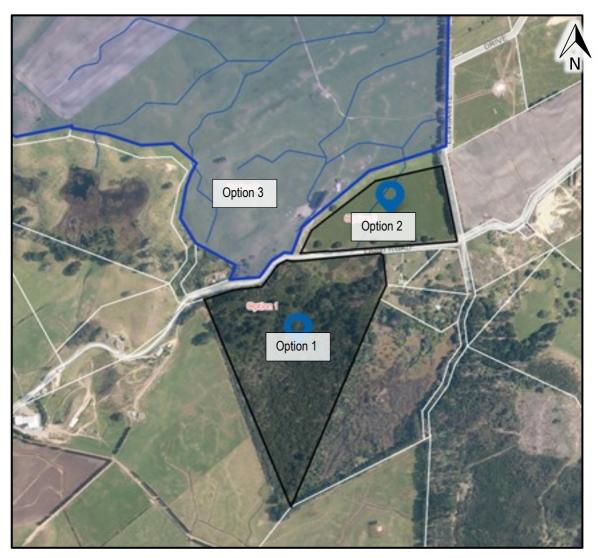


Figure 1: Aerial Image (Source: Provided by Barker Associates)

2.1 Proposed Development

A developed scheme plan was not available at the time of preparation of this report. The general proposal is a rural residential development however the final set-out and number of lots is yet to be finalised.

Hence, this report is intended to support master planning purposes, to aid in identifying potential building platforms and site constraints.

The sites (northern section of Option 1, Option 2 & Option 3) being considered for future development are shown in both Figure 1 above and Figure 2 below. The priority for the development is Option 1, in particular the ridgeline area. Depending on the number of lots, the development may extend to the Option 2 site.

Our scope is to investigate Option 3 site if Option 1 and 2 sites have large areas unsuitable for development. Based on our site walk-over inspection, Option 1 & 2 sites are considered to have sufficient areas to create multiple lots (e.g. >25, depending on lot size).

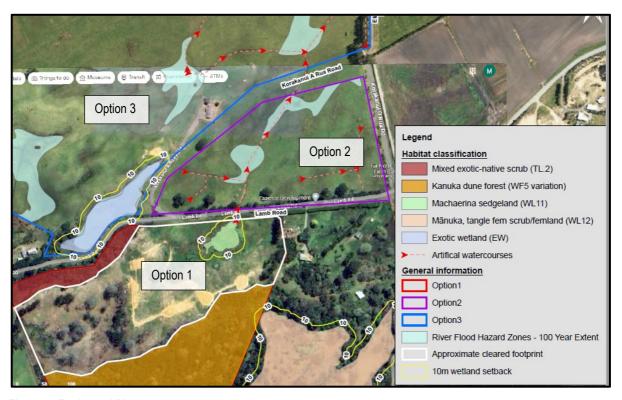


Figure 2: Ecological Plan (Source: Wild Ecology)

3.0 Geology

Reference to the GNS New Zealand Geological Web Map 1:250,000 Geology map indicates the site is underlain by dune sand deposits of the Karioitahi Group (See Figure 3). Karioitahi Group soils are described as weakly cemented sand in fixed parabolic dunes with intermixed sand, mud, and peat in interdune deposits.

Loose to cemented sands were encountered during our investigation, with no mud or peat deposits encountered (apart from augerhole AH20, which showed organic-stained sand, drilled within the wetland area).

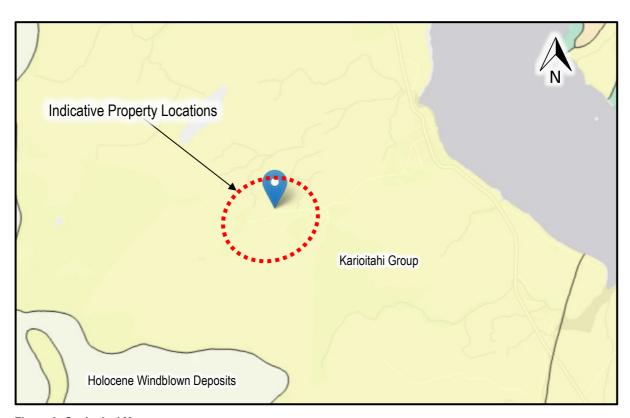


Figure 3: Geological Map (Source: GNS WebMaps Website)

4.0 Field Investigation

The field investigation carried out on 12 &13 March 2024 comprised the following components:

- Visual appraisal of the properties
- Drilling of twenty hand augerholes (AH01 AH20 inclusive) Appendix B
- Measurement of three cross section (A-A', B-B' and C-C') using measuring tape and clinometer
 Appendix A

The test locations are shown on the Site Plan, Drawing No NL230102/1 (Appendix A). The locations were determined from hand-held GPS and are therefore approximate only.

A visual-tactile field classification of the soils encountered during drilling was carried out in accordance with "Guidelines for the Field Classification and Description of Soil and Rock for Engineering Purposes", issued by the New Zealand Geotechnical Society Inc. (2005).

Measurements of undrained shear strength are normally undertaken in the augerholes at intervals of depth using a handheld shear vane in accordance with the New Zealand Geotechnical Society Guidelines for Handheld Shear Vane Tests, dated August 2001. Due to the nature of the underlying soil (sandy material), no vane shear testing was carried out in any test holes.

Dynamic Cone (Scala) Penetrometer testing was carried out in-lieu of shear vane testing where soils became sand-dominated and from the base of each augerholes until refusal or the maximum practical testing depth of the equipment was reached (i.e. AH03). Refusal is defined as five consecutive blow counts of 10 or greater per 50mm penetration or a blow count of 20 for a penetration of 50mm or less. The results are given on the attached sheet (Appendix B).

4.1 Subsurface Conditions

Subsurface conditions have been interpolated between the test locations and localised variations between and away from the test locations will exist.

In general, the soils encountered comprised Karioitahi Group soils. An outline of the soil conditions and investigation results is given below and summarised in Table 1, and detailed descriptions of the soils are given on the attached logs (Appendix B).

- Topsoil. Topsoil was not encountered in any augerholes however may be present away from the test holes.
- Non-Engineered Fill. Non-engineered fill was not encountered in any augerholes however we
 note that the material was observed to be present on the edges of the formed platforms in Option
 1 site. This material is likely to be push-over debris from the formation of building platforms and
 is not suitable for support of permanent structures (e.g. dwelling, pavement, retaining wall, etc)
- Karioitahi Group. Karioitahi Group soils were encountered at each test locations to the termination depths of the augerholes. In general, Scala penetrometer testing carried out within the Karioitahi soils recorded blow counts between 2 and 15 per 100mm penetration, indicating 'loose to dense' sands.

To confirm the depth to dense sand within the wetland feature in Option 1 site, AH20 was drilled within the wetland area. Organic-stained sand was encountered between 0.3m and 1.0m depth and immediately below (1.1m below present ground level (bpgl)) dense sand was encountered.

Sandstone/heavily-cemented sand was observed within the excavation face of the main manmade drainage in Option 2 site, refer to Figure 4 below.



Figure 4: Exposed Sandstone/Heavily-Cemented Sand (Source: S&RC Site Photo – 13 March 2024)

• Scala Penetrometer Testing. In addition to the testing within hand augerholes, Scala penetrometer testing was carried out from the base of each augerhole. Refusal, inferred to represent contact with very dense or cemented sands, was generally encountered at depths ranging between 0.2m and 1.0m below present ground level (bpgl). In AH03 and AH04 refusal was encountered at 8.0m (the maximum practical testing depth of the equipment) and 2.3m bpgl respectively. In AH20 refusal was encountered at 1.3m bpgl.

Based on the observation of the main drainage excavation, refusal in the Option 2 area is considered due to presence of the underlying sandstone/heavily-cemented sand.

Groundwater. Groundwater was not encountered in most of the augerholes on the day of drilling,
 with the exception of AH20 where groundwater was measured at 1.1m bpgl.

Groundwater measurements taken during drilling are not always an accurate portrayal of the actual long-term groundwater table as groundwater levels can take time to stabilise within the augerhole following drilling.

Rushes were observed in places, particularly within low/depressed areas. These plants thrive in wet places and generally indicate persistently wet land. Sands generally have good drainage characteristics however due the shallow sandstone/cemented sand (low permeability) surfacewater potentially ponds in low areas.

Table 1 – Summary of Subsurface Conditions

Test ID	Termination Depth	Scala Penetrometer Blow Counts (no. of blows / 100mm penetration)	Scala Penetrometer Termination		
All de	oths measured in	(m) below present ground level. (Ro	ounded to 1 DP)		
AH01	0.2	4	0.2		
AH02	0.7	2-7	1.0		
AH03	5.0	2-8	8.0		
AH04	1.8	2 – 12	2.3		
AH05	0.3	9	1.0		
AH06	0.7	3 – 8	0.7		
AH07	0.7	3 – 6	0.7		
AH08	0.8	1 – 6	0.9		
AH09	0.7	1 – 6	0.8		
AH10	0.6	2 – 5	0.8		
AH11	0.6	2 – 4	0.6		
AH12	0.5	3 – 4	0.6		
AH13	0.6	2-3	0.7		
AH14	0.7	2 – 5	0.8		
AH15	0.5	2 – 4	0.6		
AH16	0.6	2 – 3	0.6		
AH17	0.7	2 – 5	0.8		
AH18	0.5	3 – 4	0.6		
AH19	0.9	3 - 15	0.7		

Test ID	Depth 100mm p		Scala Penetrometer Termination
AH20	1.1	2 – 4	1.3

5.0 Sensitive Soils

Sandy soils (e.g. loose sand above sandstone) are potentially susceptible to mechanical disturbance and/or exposure to the elements and soils that test well in-situ can perform poorly when construction is underway. Care is therefore required during construction to ensure the soils are protected to ensure favourable short and long-term subgrade and foundation performance.

6.0 Seismic Design Parameters

The site is considered a Class C – 'Shallow Soil Site' as defined by NZS 1170.5:2004.

The Peak Ground Acceleration (PGA) value for Importance Level 2, adopted for stability analysis of the site is 0.19g (ULS) with an effective earthquake magnitude of 6.5.

7.0 Slope Stability

Qualitative Assessment - Option 1 Site

The Option 1 site comprises a broad ridgeline with side slope inclinations ranging from 20° to 30°. The geology comprises cemented dune sands.

Soil Creep is likely to be operating on these slopes. Soil creep is the slow downslope movement of upper soil horizons, usually confined to the uppermost 1.0m of soil and generally in the order of millimetres per year (or more for un-cemented sands). Soil creep is exacerbated by slope length, slope angle, inundation, groundwater fluctuations, soil expansivity, vegetation, and various surcharge loads and occurs on virtually all ground slopes. It is a normal engineering consideration and does not preclude development.

Groundwater was not encountered in any augerhole (within the elevated land) hence is unlikely to be a contributing factor to soil creep. However, surface-water runoff during times of wet or prolonged rainfall may contribute to such ground movement. Ground cover in the form of vegetation will minimise the degree of soil creep.

Concentrated stormwater of the type collected from roofs and pavements requires controlled dispersal as it represents an erosion threat if not carefully addressed. This would normally be designed as part of future residential development however any pavement associated with subdivision development should include stormwater control as part of design.

We note that a near-vertical cut, approximately 2.0m high, is present to the north of the site, along the road. The near-vertical cut appears to have been created as part of the road development and exposes cemented sand. Cemented dune sands are generally stable at steep slopes (e.g. 70°), nevertheless any permanent structure should consider the presence of any steep slopes and appropriate instability measures (e.g setbacks, pile foundations, retaining wall, etc) should be included in planning and design stage.

At the time of our investigation no visual evidence of major, deep-seated instability was identified.

Qualitative Assessment - Option 2 Site

The Option 2 site comprises very gentle ground slopes hence global instability is considered to be of no threat within the site. In any case, for future development, an appropriate setback from the main drainage channel where depth is greater than 0.6m is recommended. This is a 'local' consideration and should unduly constrain subdivision development.

Quantitative Assessment Option - 1 Site

To quantitatively check the overall stability of the slopes within the Option 1 site, computer-based stability analyses have been undertaken for the existing topography through cross sections A-A', B-B' and D-D' as indicated on the Site Plan, Drawing No. NL230102/1. Cross sections A-A' and B-B' were developed using site measurements while cross section D-D' was derived from LINZ website contour data (Lidar). These sections represent the steepest slopes within the Option 1 site.

The computer program 'SLIDE', Version 2018, developed by RocScience Inc. was used for stability calculations. Stability of theoretical translational surfaces was assessed using the Morgenstern-Price method.

No groundwater table was encountered during our investigation and given the free-draining nature of the dune sands and the preferential sheet-flow shedding characteristics related to the slopes, we consider the likelihood of a shallow standing groundwater table development to be low. Therefore, our stability analyses have been undertaken without a modelled groundwater table for the 'normal' and seismic conditions.

Furthermore, the likelihood of an extreme groundwater condition is considered highly unlikely and has not been analysed (this will, however, be required by Council if a Subdivision Consent application is made for this land).

Peak Ground Acceleration (PGA) values for the Northland Region have been determined as per Section 7.0 of this report.

As discussed above, a near-vertical cut was observed along the road. We infer that the cut is of some age and indicates the ability of the dense/cemented sand to stand unsupported at near-vertical angles. The underlying geology is likely comprised on *dense* Karioitahi Group deposits however for conservatism we modelled the upper 1.5m to 2.0m as *weathered* Karioitahi Group Soils, with lesser effective stress shear strength parameters.

Lower-bound effective stress shear strength parameters used for our analyses are summarised in Table 2. These have been developed from the soil description, in-situ strength testing, and our experience with these soil types in both the immediate area and the wider region.

Soil Type	Estimated Unit Weight γ (kN/m³)	Effective Cohesion on the Failure Plane c' (kPa)	Effective Angle of Internal Friction ø' (°)		
Weathered Karioitahi Group Soils	18	3	32		
Dense Karioitahi Group Soils	18	6	35		

Table 2 - Effective Shear Stress Parameters

The ratio of resisting forces to disturbing forces is presented as a 'Factor of Safety' (FOS) against slope instability occurring. A FOS of 1 indicates a slope near or at equilibrium.

We have adopted the following for the purposes of our assessment:

- FoS of 1.5 or higher for long-term stability when modelling the existing site conditions (measured groundwater level).
- FoS of 1.0 or higher used for short-term stability to model the effect of seismic loading.

The values above were adopted from Section 2.6.8 of the 'Auckland Council Code of Practice for Land Development and Subdivision, Chapter 2, Earthworks and Geotechnical, Version 2.0, dated May 2023 which is considered a conservative reference. The results of our analyses are provided in Table 3 below.

Table 3 – Stability Analysis Results

Section	Modelled	Global Factor of platforms at	Compliant			
	Conditions	Required	Calculated			
A-A'	Normal Groundwater	1.5	1.7	Yes		
	Seismic Loading	1.0	1.1	Yes		
B-B'	Normal Groundwater	1.5	1.6	Yes		
	Seismic Loading	1.0	1.1	Yes		
D-D'	Normal Groundwater	1.5	1.6	Yes		
_	Seismic Loading	1.0	>1.0	Yes		

Stability Conclusions

The minimum factors of safety within the potential building areas (Option 1 area, ridge top platforms) were greater than the published Council requirements (see Appendix C).

We therefore consider the potential building areas (ridge top) to be suitable for future development from a global land stability point of view contingent upon the recommendations of this report being adopted in design and construction.

The general area within the Option 2 area is also suitable for residential development from a land stability point of view.

8.0 Geotechnical Discussion

The Option 1 area (ridge top) is geotechnically suitable for residential development however slopesetbacks and/or leading-edge piles may be required depending on actual residential development proposals. Pile foundations should be expected where future dwellings are within 5.0m of any slope steeper than 14°.

The investigation within the Option 2 site indicated sandstone/cemented sand (or a very dense stratum) to be present within 1.0m bpgl. We understand that flood-prone areas are present. Geotechnically, the general Option 2 site is suitable for residential development including the flood-prone areas provided

future building platform are formed above the anticipated flood level and appropriate drainage constructed to divert surface water away from residential development.

These are geotechnical considerations and other considerations may take precedence in the overall scoping of the development.

9.0 Preliminary Geotechnical Recommendations

9.1 Cuts and Fills

Formation of roading to service future subdivision is anticipated. Within the Option 1 site, additional accessways are likely to be cut into the slopes. As discussed in Section 9.0, cemented dunes sands are generally stable at steep slopes however some form of retaining will be required if future dwelling will be situated within the influence zone of the cut. Alternatively, the dwelling may be supported on pile foundations, to transfer load below the cut's influence zone.

All fills, regardless of depth, must be placed in accordance with NZS 4431:2022 with respect to subgrade preparation and standard of compaction.

Essentially, the height of any unsupported face and proximity to building platforms and consented structures will determine the need for retaining or lower-angle battering. Any proposal to create cuts or fills greater than 1.0m in height should be the subject of specific design advice.

9.2 Retaining Structures

The following is preliminary advice provided to assist with scoping of any retaining that may be required to develop the subdivision. We anticipate that that retaining would be limited to support of cuts and fills required to form accessways.

Factors of safety and surcharge loadings appropriate to the conditions should be in accordance with 'Limit State Design of Retaining Walls and Foundations for Geotechnical and Structural Engineers' SESOC Seminar Series 2005.

We recommend retaining systems be Engineer-designed and consider both the local and global stability of the site, and any surcharge applicable to the wall. Particular attention should be paid to the influence of building surcharges above, and sloping ground above and below, any retaining wall. Geotechnical retaining wall design parameters are provided in Table 4.

Table 4 – Preliminary Retaining Wall Design Parameters

Parameter	Value
Effective Cohesion c' (kPa)	0
Internal Friction Angle (Stiff Natural Ground / Engineered Fill Only)	30°
Bulk Density (kN/m³)	18
C _u for Broms (kPa) (Stiff Natural Ground / Engineered Fill Only)	80

We have provided an 'equivalent' Cu for Broms design however 'Broms for Sand' may also be used by the designer.

For the design of 'stand-alone' timber pole retaining walls, soil pressures should be determined for <u>active</u> pressure conditions (K_a). For the design of rigid retaining walls or those that are integrated into any building structure, soil pressures should be determined for 'at-rest' pressure conditions (K_o).

Sliding resistance for a gravity wall may be calculated using a wall/ground (no plastic membrane) friction angle of 20° and the bulk density provided in Table 4.

No passive resistance should be inferred until the horizontal buttress of stiff natural soil at the downslope side of the retaining pole is at least 4D in width, where 'D' is the diameter of the bored hole. This discount recognises the lesser buttressing effect of inclined soil and also recognises the potential for soil creep and surface erosion to affect long-term pole performance,

9.3 Pavements

All topsoil, non-engineered fill, vegetation, organic or otherwise unsuitable material should be removed from under pavement areas prior to construction.

For preliminary design a CBR value of 3% or a modulus of subgrade reaction of 20kPa/mm are considered appropriate for flexible and rigid pavements respectively. These values should be confirmed by specific testing by S&RC following preparation of the subgrade.

Any pavement should be underlain by a basecourse of clean, free-draining granular fill as specified by the designer and should be subjected to compaction by a device of appropriate weight and energy. Silty or sandy subgrades are generally sensitive to disturbance and 'static' rolling only (no vibration) is recommended.

9.4 Foundation Design Recommendations – Indicative

The following is provided in order to inform likely foundation types. It is not to be used for design of foundations or support of a Building Consent.

9.4.1 Shallow Foundations

Shallow ('spread') foundations are considered suitable for the support of typical residential dwellings where within slopes flatter than 1V:4H (14°) or well clear of slopes steeper than the same.

The natural site soils are considered suitable for the use of shallow foundations which may comprise a 'waffle' or 'rib-raft' slab (surface-supported, no embedment) or traditional strip/pad/Senton footings embedded a minimum of 600mm into stiff natural ground or engineered fill.

A Design (Dependable) Bearing Capacity of 150kPa is available for Ultimate Limit State Design of shallow foundations carried out in accordance with B1/AS1 or AS2870:2011, B1/VM4 and AS/NZS 1170:2002. A Strength Reduction Factor (\emptyset_{bc}) of 0.5 has been applied to the Geotechnical Ultimate Bearing Capacity value to determine the Design Bearing Capacity.

The site soil within the general area is considered good ground in terms of NZS3604. Provided the recommended minimum foundation depth above is adopted, future dwellings may be designed using NZS3604:2011, B1/AS1 and the minimum embedment depth given above.

9.4.2 Pile Foundations

Depending on location and design of future dwellings, pile foundations may be required.

Preliminary soil strength parameters applicable to Ultimate Limit State Design in accordance with AS/NZS 1170:2002 are given in Table 5. These parameters may only be adopted for piles with a length-to-diameter ratio greater than five (L/D > 5), and that are embedded into stiff natural ground.

Table 5 – Ultimate Limit State Pile Design Parameters

Material	Ultimate End Bearing Capacity	Ultimate Skin Friction
Karioitahi Group Soils (+2.0m depth)	1,500Pa	30kPa

An 'equivalent' Cu for skin friction has been given however actual pile adhesion design should be in accordance with Section 4.1.4 (c) of B1/VM4.

A Strength Reduction Factor not greater than $\emptyset_{pc} = 0.5$ should be applied to the Geotechnical Ultimate Capacity values to determine the Design (Dependable) Capacity values.

No passive resistance should be inferred until the horizontal buttress of stiff natural soil at the downslope side of the retaining pole is at least 4D in width, where 'D' is the diameter of the bored hole. Appropriate design parameters provided in Section 10.0 of this report may be adopted to mitigate lateral pressure.

10.0 Stormwater

Concentrated stormwater flows must not be allowed to run onto or over slopes or saturate the ground as this could adversely affect slope stability or foundation conditions. Flows from all impermeable areas must be collected and carried in sealed pipes to a disposal point approved by Council.

We expect this recommendation to apply to accessway construction only at this stge. Future (individual) residential development will carry with it its own design in this respect.

11.0 On-site Wastewater Treatment and Dispersal

The encountered soils are considered suitable for the on-site dispersal of treated wastewater.

We view the near-surface soils as meeting TP58 Soil Category 3 (medium-fine and loamy sand – good drainage). However, for conservativity, we recommend Soil Category 4 (sandy loam – moderate drainage) with maximum dispersal rate of 5mm/day be adopted for future wastewater design. Given the dense, less permeable, soil at shallow depth, dispersal via conventional in-ground soakage trenches should be avoided - dispersal of treated wastewater would best be achieved via Pressure-Compensated Dripline Irrigation (PCDI).

Designers should be cognisant of groundwater depth. This could be an issue within the low-lying areas as we expect the wet-season groundwater conditions to be onerous for wastewater design. Raised dispersal beds could be a requirement. Dispersal designs should also consider overland flow features and other water bodies.

Stormwater and wastewater discharges should not interfere with each other.

12.0 Site Constraints

Below is the summary of geotechnical site constraints that should be considered in master planning.

Option 1 Site

- Generally considered suited to further residential development in geotechnical terms.
- Depending on actual location and design of future dwellings, pile foundations may be required.
 Pile foundations should be expected where future dwellings are within 5.0m of any slope steeper than 14°.
- The formation of additional accessways is likely to cut into ground slopes. As discussed in Section 9.0, cemented dunes sands are generally stable at steep slopes however some form of retaining will be required if future dwelling will be situated within the influence zone of the cut.
- Any cut or fill in excess of 1.0m height requires specific consideration and may require retaining.
- Push-over non-engineered fill (from the formation of existing platform) are present in places.
- Safe stormwater disposal related to impermeable surfaces (accessways) is a likely subdivisional requirements.
- On-site wastewater and stormwater dispersal related to future residential development proposals are achievable.

Option 2 Site

- In geotechnical terms, there are no obvious constraints to subdivision for residential purposes.
- The site is low lying with areas prone to flooding. Development within the site should consider potential flood levels.
- There could be issues with wastewater disposal if the winter and spring groundwater levels are shallow.

13.0 Future Geotechnical Assessment

Further geotechnical assessment is required following completion the final scheme prior to Resource Consent Application. Depending on the development proposal, the assessment may comprise additional investigation, drawing review and/or desktop assessment.

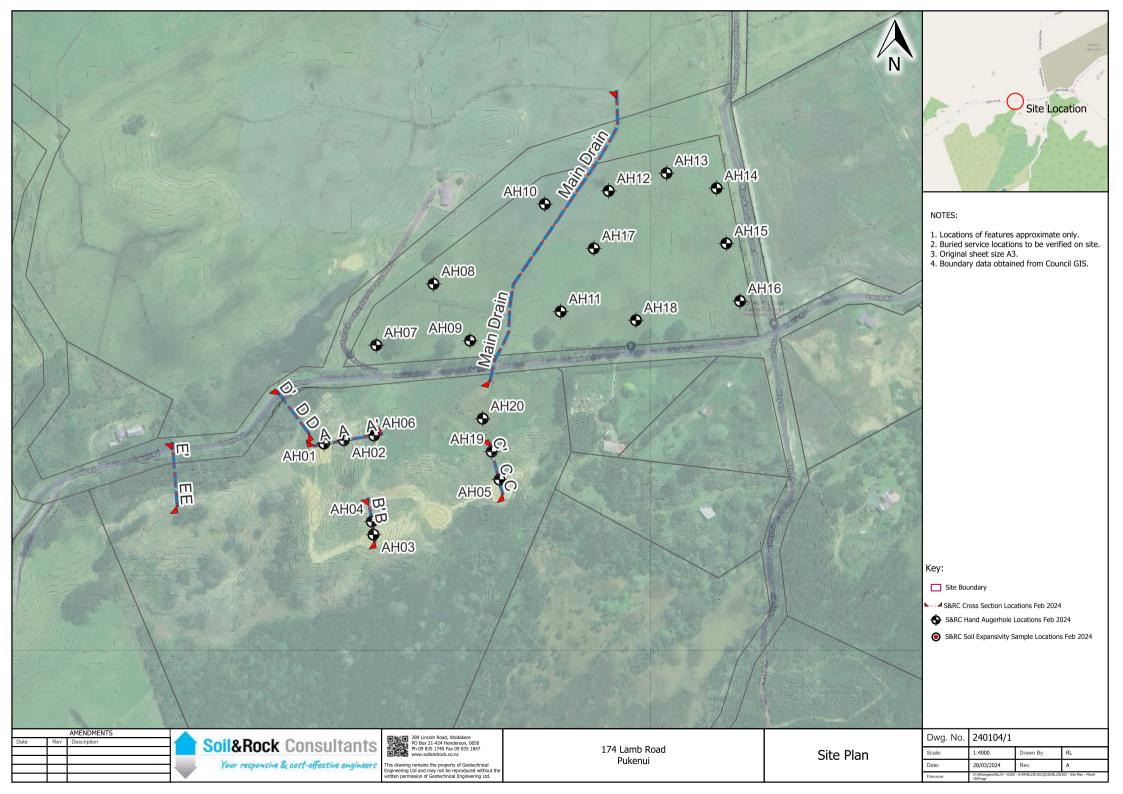
End of Report Text – Appendices Follow

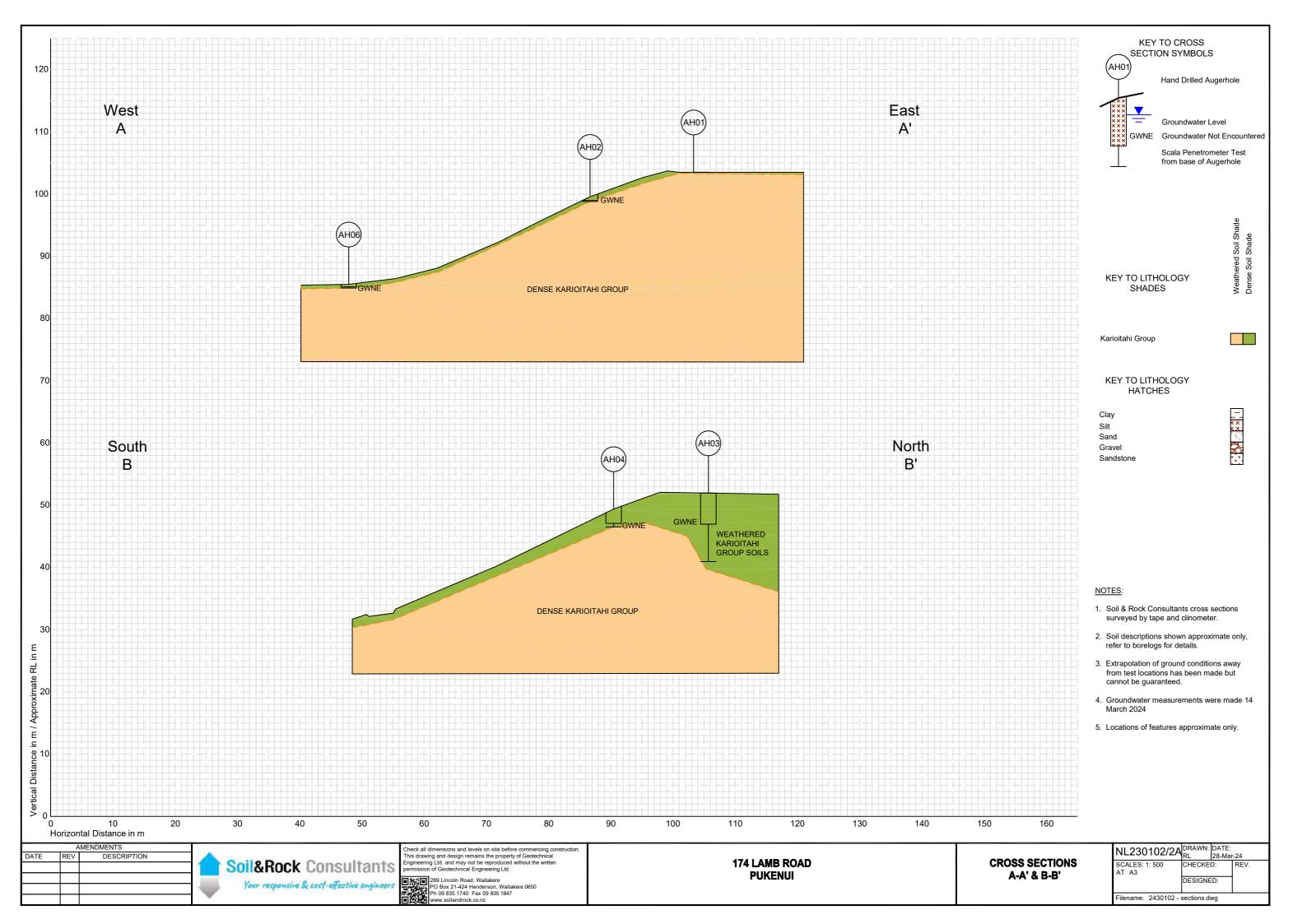


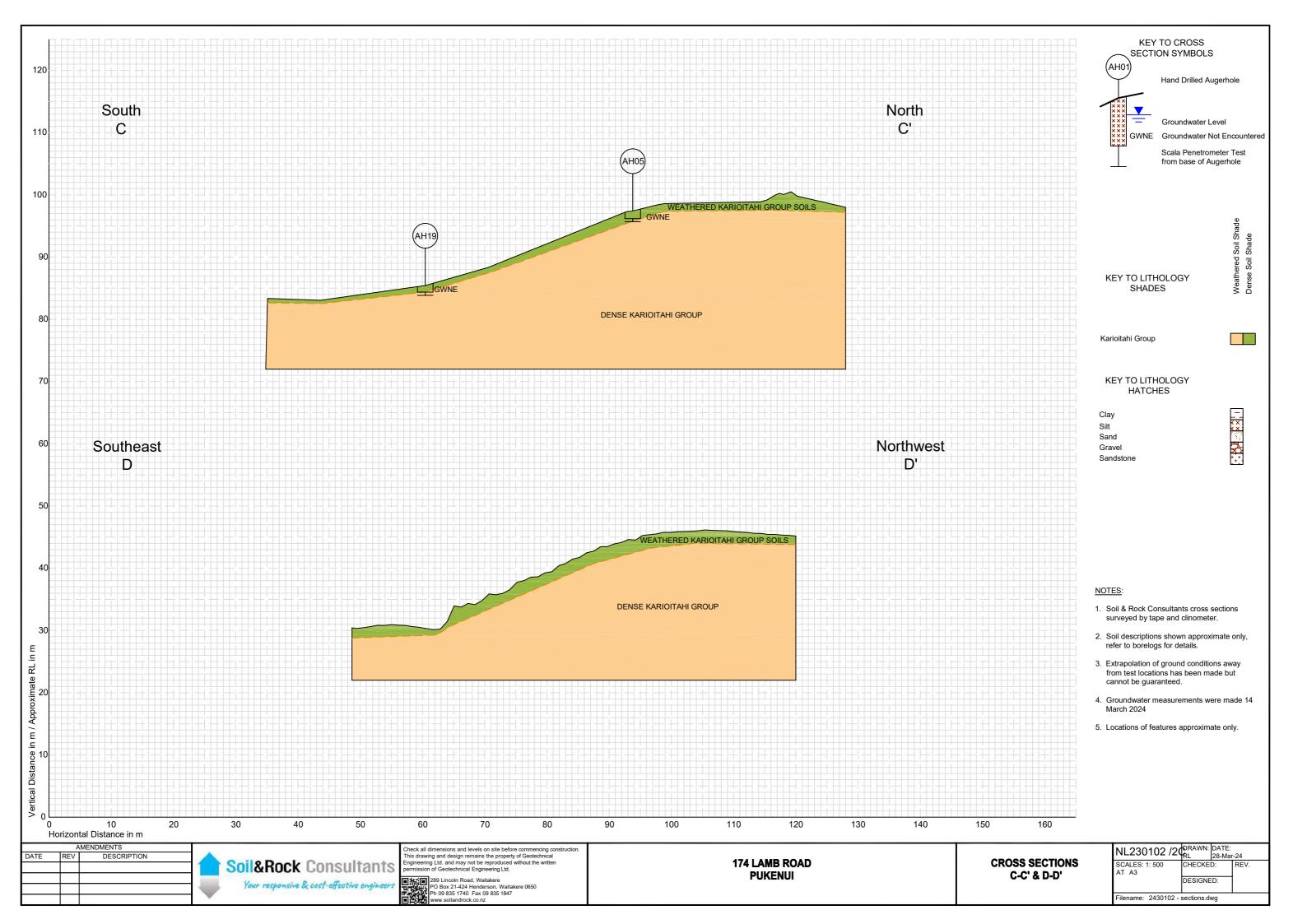
Appendix A

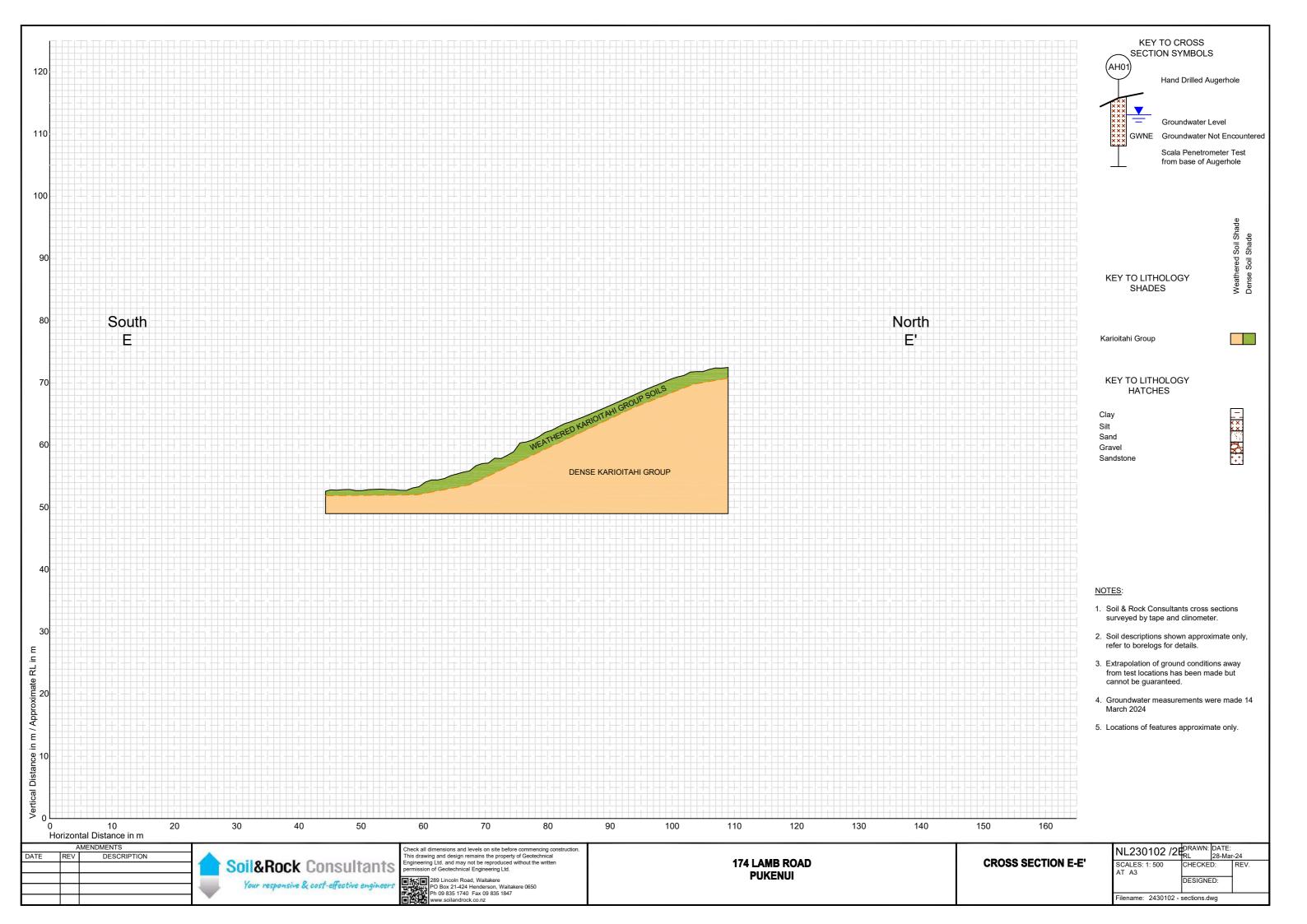
Drawings

Ref No. NL230102 Mar 2024







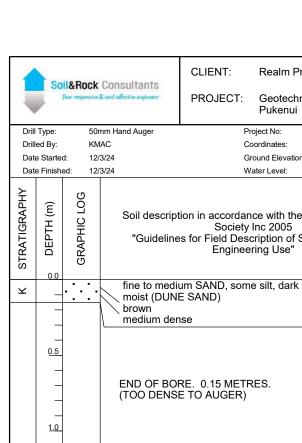




Appendix B

Investigation Logs

Ref No. NL230102 Mar 2024



HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24

Realm Property Group Ltd Auger Hole No: AH01 Geotechnical Investigation, 174 Lam Road, Sheet 1 of 1 NL230102 Logged By: JN Shear Vane No - Calibration Date: Ground Elevation: Surface Conditions: Near Level, Sand



CLIENT: Realm Property Group Ltd

Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH02

Sheet 1 of 1

F	D 111 T				B : 111 NI 000100										
	Drill T			m Hand Aug					Logged Shear V		JN	late:			
	Drilled Date :	а ву: Started	KMAC Coordinates: 12/3/24 Ground Elevation:					Shear Vane No - Calibration Date: Surface Conditions: Moderate Slope, Soil							
		Siarted Finishe		12/3/24 Water Level: Groundwater Not Encountered							. wouel	are orope, o	OII		
\vdash			12/3		Table 2010 Grownwald Hot Eliv		_		SCAL 4	DENETRO	METER TE	ет			
	<u></u>		ပ္ခ				빌	_		02:1986 te		·SI •	≿		
	AP	(E)	으	Soil d	description in accordance with the NZ Geotechnical	ļ	<u> </u>	Œ			Increment)	9 S		
	R	王l	우		Society Inc 2005	ļi	\mathbf{q}	Ξ	<u> </u>	10 2	20 ;	30 (Blows)	SAT ST(
	STRATIGRAPHY	DEPTH (m)	GRAPHIC LOG	"Gu	uidelines for Field Description of Soil and Rock in Engineering Use"		WATER LEVEL (m)	DЕРТН (m)	SHEAR	STRENGT	Ή	0 v	LABORATORY TESTS		
	2	<u>ا</u> ۵	ξ		Engineering Use"		14	DE		JLDED SHI		⊙ r	AB		
	S		o				×			50 1	00 1	50 (kPa)	_		
\vdash	\dashv	0.0	• •	fine S	SAND, some silt, light yellow brown, loose, moist			0.0	2	<u></u>					
		\dashv	`.`.\	(DUN)	NE SAND)			_	•						
	욕		` . ` .	dark	orange, medium dense			_	\ _6						
	GROUP	\dashv	• • • • •					-	5						
	5	_ +	• • • • •					_	<u> </u>						
	국	0.5	`.	dense	e			0.5	 	1	 	 			
			`. ` .	dono	•			_	····· • ⁷ ··						
\vdash			• • •					-							
		\dashv						_							
		\dashv						_	 			.			
		1.0						1.0	 	 	 	 			
		\dashv						_	 						
		\dashv		FND (OF BORE. 0.70 METRES.			-	 						
		\dashv			DENSE TO AUGER)			_							
		\dashv		,	,			_	 						
		1.5						1.5	 	ļ	 	 			
		-						_							
		\dashv						_							
		\dashv						_							
		2.0						_							
		2.0						2.0	 	ļ	 	 			
		\dashv						_							
		\dashv						_							
42		\dashv						_							
2/3/		\dashv						_							
Ĕ		2.5						2.5	 		 	 			
9.6		-						_	 						
201		-						_	 						
S+R_2013.GDT 15/3/24		\dashv						_							
		\dashv						_							
4.G		3.0						3.0							
CH2		\dashv						-	 						
AAR(4						_	 			.			
151		\dashv						-	 			.			
PS		-						-	·····						
B K		3.5						3.5	 	 	 	 			
AM		\dashv						-	 			.			
174		\dashv						-	 			.			
720		\dashv						-	 			.			
₹		\dashv						_	 						
된		4.0						4.0	 	 	 	 			
02 A		\dashv						-	 						
301(\dashv						-	 						
NE		\dashv						-	·····						
≰								_	 						
SC/		4.5						4.5	 	 	 	 			
티		\dashv						-	 						
<u>≷</u>		\dashv						-	 						
의		\dashv						_	 			.			
GER		_ +						_	 			.			
HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ		5.0						5.0	 	 	 	 			
AN P		- 1													
Ì∟															



CLIENT: Realm Property Group Ltd

PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Auger Hole No: AH03

Sheet 1 of 1

Drill Type: 50mm Hand Auger Project No: NL230102 JN Logged By: Drilled By: KMAC Coordinates: Shear Vane No - Calibration Date: Date Started: 12/3/24 Ground Elevation: Surface Conditions: Near Level, Sand 12/3/24 Date Finished: Water Level: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** DEPTH (m) DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical 10 20 30 (Blows) Society Inc 2005
"Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" ● r 150 (kPa) fine to medium SAND, some silt, grey, loose, moist (DUNE SAND) yellow orange, yellow grey, medium dense 0.5 1.0 1.0 loose medium dense loose 1.5 medium dense 2.0 2.0 KARIOITAHI GROUP HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 3.0 silty, fine to medium SAND, yellow orange, medium dense, moist <u>3.5</u> dense 4.0 4.0 medium dense dense medium dense 4.5 4.5 dense 5.0



PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Auger Hole No: AH04

Sheet 1 of 1

Drill Type: 50mm Hand Auger Project No: NL230102 JN Logged By: Drilled By: KMAC Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Moderate Slope, Sand 13/3/24 Water Level: Date Finished: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 20 Society Inc 2005 "Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" • r 150 (kPa) fine SAND, minor silt, yellow orange, medium dense, moist (DUNE SAND) yellow orange, some black speckles 0.5 light brown orange, loose KARIOITAHI GROUP some silt, medium dense 1.0 dense 10 10 silty SAND, orange brown, yellow orange speckles, dense, 1.5 •12 2.0 END OF BORE. 1.80 METRES. HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 (TOO DENSE TO AUGER) 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH05

Drille Date	Type: ed By: e Started: e Finished	SMI : 12/3	3/24	Coordinates: Ground Elevation:	NL230102 Groundwater Not Encount	tered				DEG alibration D : Moder	ate: ate Slope, G	irass
STRATIGRAPHY	o DEPTH (m)	GRAPHIC LOG		tion in accordance with the NZ (Society Inc 2005 es for Field Description of Soil a Engineering Use"		WATER LEVEL (m)	OEPTH (m)	NZS:440 (Blows p 1 SHEAR REMOU	02:1986 tes per 100mm 0 2 STRENGT ILDED SHE	Increment) 20 3 TH EAR	•	LABORATORY TESTS
×			subrounded (DUNE SAN	um SAND, trace silt, some fine l gravel, orange, yellow, red bro VD) ark orange, orange red, dense	to coarse wn, loose, dry		_	•••••••	9			
	0.5	• •	no gravei, u	ant drange, drange red, dense			0.5					
			END OF BO (TOO DENS	RE. 0.30 METRES. E TO AUGER)			_ _ _ 1.0					
	1.5 —						1.5 —					
	2.0						 2.0					
	_ _ _ _						-					
	<u>2.5</u> 						<u>2.5</u> 					
	3.0						3.0					
	3.5						3.5					
							_ _ _					
	4.0						4.0 —					
	4.5						 4.5 					
	5.0											
	9.0						<u>0.0</u>					



PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Sheet 1 of 1

Auger Hole No: AH06

Drill Type: 50mm Hand Auger Project No: NL230102 JN Logged By: Drilled By: KMAC Coordinates: Shear Vane No - Calibration Date: Date Started: 12/3/24 Ground Elevation: Surface Conditions: Near Level, Grass 12/3/24 Date Finished: Water Level: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 Society Inc 2005 "Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" ● r 150 (kPa) fine to medium SAND, some silt, dark yellow, loose, moist (DUNE SAND) brown, grey brown, medium dense K. GROUP dense medium dense trace tree roots, dark brown 0.5 1.0 END OF BORE. 0.65 METRES. (TOO DENSE TO AUGER) 1.5 2.0 HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Auger Hole No: AH07

Sheet 1 of 1

Drill Type: 50mm Hand Auger Project No: NL230102 Logged By: DEG Drilled By: SMB Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Slight Slope, Grass 13/3/24 Date Finished: Water Level: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 Society Inc 2005
"Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" ● r 150 (kPa) fine SAND, minor silt, brown, grey, loose, moist (DUNE SAND) medium dense trace silt K. GROUP 0.5 dark red brown 1.0 END OF BORE. 0.65 METRES. (TOO DENSE TO AUGER) 1.5 2.0 HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Auger Hole No: AH08

Sheet 1 of 1

Drill Type: 50mm Hand Auger Project No: NL230102 DEG Logged By: Drilled By: SMB Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Slight Slope, Grass 13/3/24 Date Finished: Water Level: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 Society Inc 2005
"Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" • r 150 (kPa) fine SAND, minor silt, brown, light brown, very loose, moist (DUNE SAND) KARIOITAHI G brown, loose trace silt, grey medium dense 0.5 some silt, dark brown dark brown, brown, red brown 1.0 END OF BORE. 0.80 METRES. (TOO DENSE TO AUGER) 1.5 2.0 HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH09

	Type: ed By:	50n SMI	nm Hand Auger	Project No: NL230102 Coordinates:				Logged E	By: ane No - C	DEG alibration		
Date	e Started e Finishe	d: 13/3	3/24	Ground Elevation: Water Level: Groundwater Not En	countered	i			Conditions		nt Slope, Gras	S
STRATIGRAPHY	DEPTH (m)	GRAPHIC LOG		tion in accordance with the NZ Geotechnical Society Inc 2005 es for Field Description of Soil and Rock in Engineering Use"	WATER LEVEL (m)	חבסבת (יייי)		NZS:440 (Blows p	PENETRO 02:1986 te per 100mm 0 2 STRENGT	st 6.5.2 Incremer 20	0	LABORATORY TESTS
တ	0.0		fine CAND	Annea eile limbe breaum Leann mariae (DUNE	× ×	(0.0	5	0 1	100	150 (kPa)	
KARIOITAHI G			SAND)	trace silt, light brown, loose, moist (DUNE ht grey, medium dense rey brown			-	2				
KARI	0.5					(0.5	5				
		• •	red brown		_		7					
	1.0						1.0					
			END OF BO	RE. 0.65 METRES.			-					
			(TOO DENS	E TO AUGER)								
	<u>1.5</u>						1.5					
							-					
	2.0					1	2.0					
]					
	 2.5					;	2.5					
							-					
	_						- - - - - - - - - - - -					
	<u>3.0</u>					,	3.0					
							- - - - - - - - - - - -					
	 3.5					,	3.5			+		
							+					
							-					
	4.0					1	4.0					
							7					
	<u>4.5</u>					4	4.5			1		
]					
	5.0						5.0					
						'						



PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Auger Hole No: AH10

Sheet 1 of 1

Drill Type: 50mm Hand Auger Project No: NL230102 Logged By: DEG Drilled By: SMB Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Slight Slope, Grass 13/3/24 Date Finished: Water Level: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 20 Society Inc 2005
"Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" ● r 150 (kPa) fine SAND, minor silt, brown, loose, moist medium dense K. GROUP trace silt, grey, brown 0.5 dark red brown 1.0 END OF BORE. 0.60 METRES. (TOO DENSE TO AUGER) 1.5 2.0 HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH11

Drille Date	Type: led By: e Started:	SMI : 13/3	3/24	Project No: NL230102 Coordinates: Ground Elevation:				By: ane No - C Conditions		Date: Slope, Grass	3
STRATIGRAPHY	e Finished (m) DEPTH (m) 0.0	d: 13/2 GRAPHIC LOG	Soil descrip	Water Level: Groundwater Not E tion in accordance with the NZ Geotechnical Society Inc 2005 es for Field Description of Soil and Rock in Engineering Use"	ed (III) AN EN	DEPTH (m)	NZS:44 (Blows p 1 SHEAR REMOU	STRENGT JLDED SHI	st 6.5.2 Increment 20 TH EAR	•	LABORATORY TESTS
K. GROUP	• • •		medium der	some silt, brown, loose, moist (DUNE SAND) nse ht grey, grey		- - - - 0.5	3 3 3				
			END OF BO	RE. 0.55 METRES. F TO AUGER)							
	1.5 —		(TOO DENS	E TO AUGER)		 1.5 					
	2.0 ————————————————————————————————————										
	2.5 ————————————————————————————————————										
	3.0 — — — — — 3.5					3.0 - - - - 3.5					
						- - - 4.0					
	 4.5					_ _ _ 4.5					
						5.0					



HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24

CLIENT: Realm Property Group Ltd

PROJECT: Geotechnical Investigation, 174 Lam Road,

Sheet 1 of 1

Auger Hole No: AH12

Pukenui Drill Type: 50mm Hand Auger Project No: NL230102 Logged By: DEG Drilled By: SMB Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Slight Slope, Grass 13/3/24 Date Finished: Water Level: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 Society Inc 2005
"Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" ● r 150 (kPa) fine SAND, minor silt, brown, loose, moist (DUNE SAND) GROUP trace silt, dark grey, brown, medium dense brown, dark red brown 1.0 END OF BORE. 0.50 METRES. (TOO DENSE TO AUGER) 1.5 2.0 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24

CLIENT: Realm Property Group Ltd

PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Auger Hole No: AH13
Sheet 1 of 1

Drill Type: 50mm Hand Auger Project No: NL230102 DEG Logged By: Drilled By: SMB Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Slight Slope, Grass 13/3/24 Water Level: Date Finished: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 Society Inc 2005
"Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" ● r 150 (kPa) fine SAND, minor silt, brown, dark brown, loose, moist (DUNE SAND) K. GROUP dark grey, grey, medium dense trace silt loose 0.5 dark red brown 1.0 END OF BORE. 0.60 METRES. (TOO DENSE TO AUGER) 1.5 2.0 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Sheet 1 of 1

Auger Hole No: AH14

Drill Type: 50mm Hand Auger Project No: NL230102 Logged By: DEG Drilled By: SMB Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Slight Slope, Grass 13/3/24 Date Finished: Water Level: Groundwater Not Encountered SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 Society Inc 2005
"Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" • r 150 (kPa) fine SAND, minor silt, brown, loose, moist (DUNE SAND) KARIOITAHI G light grey, brown, medium dense trace silt 0.5 dark red brown 1.0 END OF BORE. 0.65 METRES. (TOO DENSE TO AUGER) 1.5 2.0 HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH15

	ill Type: illed By:	50n SM	nm Hand Auger B		oject No: oordinates:	NL230102			Logged Shear V	By: 'ane No - Ca	DEG alibration D	ate:	
	ate Started ate Finishe		3/24 3/24		ound Elevation: ater Level:	Groundwater Not End	countered	ı	Surface	Conditions:	Slight	Slope, Gras	S
STRATIGRAPHY	DEPTH (m)	GRAPHIC LOG	Soil descript	ion in accordan	ce with the N Inc 2005 cription of So	Z Geotechnical	WATER LEVEL (m)	DEPTH (m)	NZS:44 (Blows	PENETRO 102:1986 tes per 100mm 10 2 R STRENGT JLDED SHE	st 6.5.2 Increment) 20 3	•	LABORATORY TESTS
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.0		fine SAND	minor silt brown	loose mois	st (DUNE SAND)		0.0	· · · · · · · · · · · · · · · · · · ·	50 1	00 1	50 (kPa)	_
GROUP				medium dense		SE (DOINE OAIND)		-	3				
	-		trace silt					-	3				
ᅶ	0.5		red brown, c	lark red brown				0.5					
								-					
								-					
	1.0		END OF BOR	RE. 0.50 METR E TO AUGER)	RES.			1.0					
			`	,				-	<u> </u>				
	<u>1.5</u>							1.5					
								-	<u> </u>				
								-]				
	2.0							2.0					
								-					
3/24								-	<u> </u>				
2013.GDT 15/3/24	2.5							2.5					
2013.G								-					
S + R								-	-				
ROAD 15MARCH24.GPJ	3.0							3.0					
MARCH								-	<u> </u>				
OAD 15								-	-				
AMB R	<u>3.5</u>							3.5					
- AH20 174 LAMB								-	1				
1 - AH2(-					
12 AH01	4.0							4.0	<u> </u>				
L23010								-	<u> </u>				
SCALA NL230102 AH01	<u>4.5</u>							4.5					
WITH SC								-	-				
100 v								-]				
AUGER LOG WITH	<u>5.0</u>							5.0	<u> </u>				
HAND /													



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH16

Drille Date	I Type: led By: e Started: e Finished	SMI : 13/3	3/24	Project No: NL230102 Coordinates: Ground Elevation: Water Level: Groundwater No	ot Encounte	ered			By: ane No - Ci		oate: Slope, Grass	;
STRATIGRAPHY	o DEPTH (m)	GRAPHIC LOG		tion in accordance with the NZ Geotechnic Society Inc 2005 es for Field Description of Soil and Rock in Engineering Use"	al	WATER LEVEL (m)	OEPTH (m)	NZS:444 (Blows p 1 SHEAR REMOU	STRENGT ILDED SHE	st 6.5.2 Increment 20 : TH EAR	•	LABORATORY TESTS
K. GROUP				trace silt, brown, loose, moist (DUNE SAN medium dense	D)		- - -	3 3				
	0.5 • — — —	•	red blown				0.5 - - -					
	1.0 ————————————————————————————————————		END OF BO (TOO DENS	RE. 0.55 METRES. E TO AUGER)			1.0 - - -					
	1.5 ————————————————————————————————————						1.5 - - -					
	2.0 — — — —						<u>2.0</u> - - -					
	2.5 — — — —						<u>2.5</u> - - -					
	3.0						3.0 - - -					
	3.5 — — —						3.5 - - -					
	4.0 — — —						4.0 - -					
	4.5 — — —						4.5 - -					
	<u>5.0</u>						<u>-</u> 5.0					



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH17

	Type: ed By:	50m KM/	nm Hand Auger	Project No: NL230102 Coordinates:				Logged I	By: ane No - C	JN alibration	Date:	
Date	e Started: e Finished	13/3	3/24	Ground Elevation: Water Level: Groundwater Not End	countered	ii			Conditions		r Level, Grass	
STRATIGRAPHY	DEPTH (m)	GRAPHIC LOG		tion in accordance with the NZ Geotechnical Society Inc 2005 es for Field Description of Soil and Rock in Engineering Use"	WATER LEVEL (m)	OEDTH (m)		NZS:440 (Blows p	PENETRO 02:1986 tes per 100mm 0 2 STRENGT	st 6.5.2 Incremei 20	•	LABORATORY TESTS
ST	0.0	ō			WA		0.0	5		00	150 (kPa)	
K. GROUP	• • • 0.5		moist (DUN) medium der			(0.5	2 4 5 4 4				
	-		some silt, da	ark red brown			+	•4				
	1.0						1.0					
			END OF BO	RE. 0.65 METRES.			1					
	 1.5		(TOO DENS	E TO AUGER)			1.5					
	2.0						2.0					
	_						4					
	 2.5						2.5					
	3.0						3.0					
	_											
	 3.5						3.5					
	- 4.0					4	4.0					
	4.5					4	4.5					
							-					
	 5.0						5.0					
						`						



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH18

Project No:	NL230102	Logged By: JN	
Coordinates:		Shear Vano No. Calibration Date:	

- 1	ill Type:	50mm Hand Auger	Project No:	NL230102			Logged E		JN		
	illed By: ite Started:	KMAC 13/3/24	Coordinates: Ground Elevation:					ane No - Ca Conditions:		ate: evel, Grass	
	ite Started. ite Finished:	13/3/24	Water Level:	Groundwater Not Encoun	itered		Suriace	Jonaillons.	iveai Li	evei, Grass	
STRATIGRAPHY	DEPTH (m)		cription in accordance with the N Society Inc 2005 elines for Field Description of Soi Engineering Use"	Z Geotechnical	WATER LEVEL (m)	DEPTH (m)	NZS:440 (Blows p	STRENGTI LDED SHE	t 6.5.2 Increment) 0 3 H	•	LABORATORY TESTS
K. GRP	0.0	dense, r	ND, minor silt, dark grey, white sp moist (DUNE SAND) ey, brown t, dark red brown	eckles, medium		0.0	4			00 (KFA)	
ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24	1.0 	END OF	BORE. 0.45 METRES. ENSE TO AUGER)			0.5 					
HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB R	3.5 					3.5 - - 4.0 - - - - - - - - - - - - - - - - - - -					
HAN			289 Lincoln Road, H		0.65=						



Geotechnical Investigation, 174 Lam Road, Pukenui PROJECT:

Auger Hole No: AH19

				i ukcilui								
Drill	Type:	50n	nm Hand Auger	Project No: NL23	30102			Logged I	By:	DEG		
Drill	ed By:	SMI	В	Coordinates:				Shear Va	ane No - Ca	alibration [ate:	
Dat	e Started	d: 12/3	3/24	Ground Elevation:				Surface	Conditions:	Slight	Slope, Grass	;
Dat	e Finishe	ed: 12/3	3/24	Water Level: Grou	indwater Not Encount	ered						
						<u></u>		SCALA	PENETRO	METER TE	ST	
Ţ	_	90				<u>-</u>	_	NZS:440	02:1986 tes	st 6.5.2	•	≿
A	E)	\preceq	Soil descript	ion in accordance with the NZ Geo	ntechnical	Ē	E)		er 100mm			9 S
K	ᅵᆮᅵ	유		Society Inc 2005		Щ	프	1	0 2	20	30 (Blows)	ST.
STRATIGRAPHY	DЕРТН (m)	GRAPHIC LOG	"Guideline	es for Field Description of Soil and Engineering Use"	Rock in	WATER LEVEL (m)	DЕРТН (m)	SHFAR	STRENGT	Ή	0 v	LABORATORY TESTS
≱	👸	№		Engineering Use"		쁘ㅣ	DE		LDED SHE		⊙ r	AB.
S		Ö				≸ l		_			50 (15)	J.
-	0.0		fine SAND	trace silt, light brown, medium dens		_	0.0		0 1	00 1	50 (kPa)	
		• • • •	(DUNE SAN	inace sin, light brown, mediam dens ID)	se, moisi		_	• ³				
Ι.	l ⊣			,			_	3				
9			light grey					3				
∓			light grey, bu	rown]3	[
	0.5						0.5	\ 4				
KARIOITAHI G		[light grey, de	ense					_11			
₹		. • . • . 1	white						12			
-	l T	· · · ·					_		∤ @			
		· · · · ·	minor silt. lic	ght grey, light brown			_		15			
		• • •	brown	, , , ,	J		_					
	1.0		,		/		1.0	·	 		+	
							_					
							_				.	
							_				.	
	1.5		END OF BOI	RE. 0.90 METRES.			1.5			L		
			(TOO DENS	E TO AUGER)								
	П						_					
							_					
	-						-					
	-						_					
	2.0						2.0				 	
							_					
							_					
4							_					
/3/2												
15	2.5						2.5					
.+R_2013.GDT 15/3/24												
13.0												
2												
¥							_					
2							_					
4. Q	3.0						3.0				+	
HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S	-						_				· ·····-	
AR AR	-						-				+	
15N	-						_				.	
Q Q	-						_				.	
2	3.5						3.5		ļ			
AME											.	
4 [.	
0 17	_]						_		l]]	
ξ	Ι٦								l	l	1	
[4.0						4.0		[[1	
위							0		· · · · · · · · · · · · · · · · · · ·	<u> </u>	T	
05,							-				1	
301							_				· ·····-	
N N							-				· · · · · · · · · · · · · · · · · · ·	
⊴	-						-				+	
٥ ک	4.5						4.5	L	ļ	 	 	
뙨							_				.	
×							_				.	
90									 			
띪	_]								l		1	
힝	5.0						5.0		[[
ğ	"						0.0		· · · · · · · · · · · · · · · · · · ·	1	T	
Ĭ M												
┸┖──									l			



PROJECT: Geotechnical Investigation, 174 Lam Road,

Pukenui

Auger Hole No: AH20

Sheet 1 of 1

Drill Type: 50mm Hand Auger Project No: NL230102 DEG Logged By: Drilled By: SMB Coordinates: Shear Vane No - Calibration Date: Date Started: 13/3/24 Ground Elevation: Surface Conditions: Slight Slope, Grass 13/3/24 Date Finished: Water Level: 1.10m 13/3/24 SCALA PENETROMETER TEST Ξ STRATIGRAPHY LABORATORY TESTS **GRAPHIC LOG** NZS:4402:1986 test 6.5.2 **WATER LEVEL** Ξ DEPTH (m) (Blows per 100mm Increment) Soil description in accordance with the NZ Geotechnical DEPTH (30 (Blows) 10 Society Inc 2005 "Guidelines for Field Description of Soil and Rock in SHEAR STRENGTH REMOULDED SHEAR Engineering Use" ● r 150 (kPa) fine SAND, minor silt, dark brown grey, orange speckles, loose, moist (DUNE SAND) fine SAND, some organic silt, black with orange speckles, KARIOITAHI G loose, wet medium dense black, dark red brown 1.0 fine to medium SAND, some silt, red brown, medium dense, saturated 1.5 END OF BORE. 1.10 METRES. (TOO DENSE TO AUGER) 2.0 HAND AUGER LOG WITH SCALA NL230102 AH01 - AH20 174 LAMB ROAD 15MARCH24.GPJ S+R_2013.GDT 15/3/24 2.5 3.0 3.5 4.0 4.0 4.5 4.5 5.0 5.0





SCALA PENETROMETER SHEET - TABLE OF BLOWS PER INCREMENT

JOB NO: NL230102 TESTED BY: DEG, JN, KMAC, SMB

JOB NAME: 174 Lamb Road, Pukenui DATE: 12-13/3/24

Depth of												
Penetration [mm]	AH01	AH02	AH03	cont	AH04	AH05	AH06	AH07	AH08	AH09	AH10	AH11
DEPTH START[m]	0.15	0.70	5.00	7.00	1.80	0.30	0.65	0.65	0.80	0.65	0.60	0.55
50 mm	20+	7	4	5	7	6	20+	20+	20+	19	8	20+
100		10	3	5	9	7				20+	11	
150		12	4	4	10	7					20+	
200		10	4	5	8	11						
250		10	4	6	9	12						
300		10	4	5	10	11						
350			3	4	10	12						
400			2	5	10	13						
450			2	5	10	10						
500			2	6	10	11						
550			2	6		12						
600			3	7		12						
650			3	6		12						
700			4	6								
750			4	6								
800			4	8								
850			6	7								
900			5	6								
950			6	6								
1000			5	6								
1050			4									
1100			4									
1150			4									
1200			4									
1250			5									
1300			4									
1350			4									
1400			3									
1450			6									
1500			5									
1550			4									
1600			5									
1650			5									
1700			4									
1750			5									
1800			6									
1850			6									
1900			5									
1950			7									
2000			5									
DEPTH END [m]	0.20	1.00	7.00	8.00	2.30	0.95	0.70	0.70	0.85	0.75	0.75	0.60

Testing Method: NZS 4402:1988 Test 6.5.2 Dynamic Cone Penetrometer





SCALA PENETROMETER SHEET - TABLE OF BLOWS PER INCREMENT

JOB NO: NL230102 TESTED BY: DEG, JN, KMAC, SMB

JOB NAME: 174 Lamb Road, Pukenui DATE: 12-13/3/24

Depth of											
Penetration [mm]	AH12	AH13	AH14	AH15	AH16	AH17	AH18	AH19	AH20		
•											
DEPTH START[m]	0.50	0.60	0.70	0.50	0.50	0.65	0.45	0.90	1.20		
50 mm	20+	16	20+	20+	20+	5	10	20+	12		
100		20				20+	20+		20+		
150											
200											
250											
300											
350											
400											
450											
500											
550											
600											
650											
700											
750											
800											
850											
900											
950											
1000											
1050											
1100											
1150											
1200											
1250											
1300											
1350											
1400											
1450											
1500											
1550											
1600											
1650											
1700											
1750											
1800											
1850											
1900											
1950											
2000											
DEPTH END [m]	0.55	0.70	0.75	0.55	0.55	0.75	0.55	0.70	1.30		

Testing Method: NZS 4402:1988 Test 6.5.2 Dynamic Cone Penetrometer



Appendix C

Slope Stability Results

Ref No. NL230102 Mar 2024

